

10/2 L1

Linear Spaces & Operators:

$x \in \mathbb{R}^n$  linear space

$\forall x_1, x_2 \in \mathbb{R}^n$

$\forall \alpha_1, \alpha_2 \in \mathbb{R} \quad \alpha_1 x_1 + \alpha_2 x_2 \in \mathbb{R}^n$

Linear space  $V$

-  $V$  is a set

- Addition;  $v_1, v_2 \in V \rightarrow v_1 + v_2 \in V$

- Scaling over  $\mathbb{F}$ :  $v \in V, \alpha \in \mathbb{F} \rightarrow \alpha v \in V$

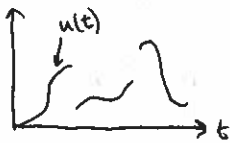
-  $0 \in V$  s.t.  $v + 0 = v$

-  $1 \in \mathbb{F}$  s.t.  $1v = v$

intervals of finite duration finite # of discontinuities

Ex:  $V = P[0, T]$  ~ signals, piecewise cont. on  $[0, T]$

$u(\cdot) \in P[0, T]$  over  $\mathbb{R}$  field



$u_1(\cdot) + u_2(\cdot) = (u_1 + u_2)(\cdot)$   
 $u: T \rightarrow V$

$\hookrightarrow$  so dimensional because it's continuous on  $[0, T]$

zero element:  $0(\cdot) \rightsquigarrow 0(t) = 0 \in \mathbb{R}$

Ex:  $V = P[0, \infty)$

Ex:  $V = C^n[0, T]$   $n$ -differentiable cont. function



Norms of signals:

$\|\cdot\| \quad u(\cdot) \in \mathcal{V} \quad \|\cdot\|: \mathcal{V} \rightarrow \mathbb{R}$

satisfies: a)  $\|u(\cdot)\| \geq 0 \quad \forall u(\cdot) \in \mathcal{V}$

b)  $\|u(\cdot)\| = 0$  iff  $u(\cdot) = 0$

c)  $\|u(\cdot) + v(\cdot)\| \leq \|u(\cdot)\| + \|v(\cdot)\|$

d)  $\|\alpha u(\cdot)\| = |\alpha| \|u(\cdot)\|$

Ex:  $v \in \mathbb{R}^n$

$\|v\|_2 = \sqrt{v_1^2 + \dots + v_n^2}$

$u(\cdot) \in \mathcal{V}$   
 $\|u(\cdot)\|_2 = \left( \int_0^T \|u(\tau)\|^2 d\tau \right)^{1/2}$

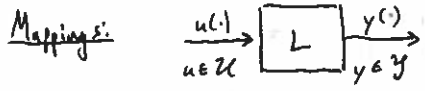
\* Try to show c) on  $\uparrow$

Extends to  $p$ -norm:

$\|u(\cdot)\|_p = \left( \int_0^T \|u(\tau)\|^p d\tau \right)^{1/p}$

$\|u(\cdot)\|_\infty = \max_{\tau \in [0, T]} \|u(\tau)\|$   
 $= \sup_{t \in T} \|u(t)\|$

Ex:  $T = [0, \infty)$   $u(t) = 1 - e^{-t}$ ,  $\sup = 1$



$y(\cdot) = L(u(\cdot)) \quad L: \mathcal{U} \rightarrow \mathcal{Y}$

$L$  is a linear operator if:

a)  $L(u_1 + u_2) = L(u_1) + L(u_2)$

b)  $L(\alpha u_1) = \alpha L(u_1)$

Ex: Time delay (not finite dimensional, but still linear)

$\bullet Av = \int_0^1 v(t) dt, v \in C[0, 1]$

$A: C[0, 1] \rightarrow \mathbb{R}$

Given:  $h \in C[0, \infty), v \in C[0, \infty)$

$(L_h v)(t) = \int_0^t h(t-\tau)v(\tau) d\tau$

$L_h: C[0, \infty) \rightarrow C[0, \infty)$

} impulse response

Dynamical System:  $\mathcal{D} = (\mathcal{U}, \Sigma, \mathcal{Y}, S, r)$   
 on  $T \subset \mathbb{R}$  (time interval)

$x$  is  $\Sigma$  in input space of signals  
 $\dot{x} = Ax + Bu$   
 $y = Cx$

$\rightarrow$  read out map

$\leftarrow$  state update map

output space of signals

Update map:  $s(t_1, t_0, x_0, u(\cdot)) =$  state at time  $t_1$  given that state at  $t_0 = x_0$  & apply  $u(t), t \in [t_0, t_1]$

$s \in \Sigma: T \times T \times \Sigma \times \mathcal{U} \rightarrow \Sigma$

a) State transition axiom: If two signals  $u(\cdot)$  &  $\tilde{u}(\cdot)$  agree on  $T$ , then  $s(t_1, t_0, x_0, u(\cdot)) = s(t_1, t_0, x_0, \tilde{u}(\cdot))$

$\forall t \in [t_0, t_1]$   
 $\hookrightarrow u(t) = \tilde{u}(t) \quad \forall t \in T = [t_0, t_1]$

b) Semi-group:

$s(t_2, t_1, s(t_1, t_0, x_0, u(\cdot)), u(\cdot)) = s(t_2, t_0, x_0, u(\cdot))$

10/4 L2: Impulse Response:

• zero state response ( $x_0 = 0$ ) to  $u(t)$

$G(t): y(t) = \int_{-\infty}^{\infty} G(t-\tau)u(\tau) d\tau := G * u$

• Laplace transform:  $y(t) \rightarrow \hat{Y}(s)$

$\hat{Y}(s) = \int_0^{\infty} y(t) e^{-st} dt$

Now we will plug in the zero state response,

$\hat{Y}(s) = \int_0^{\infty} \left( \int_0^{\infty} G(t-\tau)u(\tau) d\tau \right) e^{-st} dt$   
 $= \int_0^{\infty} \left( \int_0^{\infty} G(t-\tau) e^{-st} dt \right) u(\tau) d\tau$   
 $= \int_0^{\infty} \left( \int_0^{\infty} G(t-\tau) e^{-s(t-\tau)} d(t-\tau) \right) u(\tau) e^{-s\tau} d\tau \dots \tilde{t} = t-\tau$   
 $= \int_0^{\infty} \left( \int_0^{\infty} G(\tilde{t}) e^{-s\tilde{t}} d\tilde{t} \right) u(\tau) e^{-s\tau} d\tau$   
 $= \underbrace{\left( \int_0^{\infty} G(\tilde{t}) e^{-s\tilde{t}} d\tilde{t} \right)}_{\hat{G}(s)} \underbrace{\left( \int_0^{\infty} u(\tau) e^{-s\tau} d\tau \right)}_{\hat{U}(s)}$

$\hat{Y}(s) = \hat{G}(s) \hat{U}(s) \equiv \hat{G}_{1 \times 1}(s) \hat{U}(s)$

Norms of system (siso)

$$\|\hat{G}\|_2 = \left( \frac{1}{2\pi} \int_{-\infty}^{\infty} |\hat{G}(j\omega)|^2 d\omega \right)^{1/2}$$

$$\|\hat{G}\|_{\infty} = \sup_{\omega} |\hat{G}(j\omega)|$$

Parseval's theorem:  $\|\hat{G}(s)\|_2^2 = \int_{-\infty}^{\infty} |G(t)|^2 dt = \|G(t)\|_2^2$

(oo-norm)  $\|\hat{G}\hat{H}\|_{\infty} \leq \|\hat{G}\|_{\infty} \|\hat{H}\|_{\infty}$

state space:

$$\dot{x} = Ax + Bu, \quad y = Cx + Du$$

$$\hat{G}(s) = C(sI - A)^{-1}B + D \quad (\text{from } \mathcal{L})$$

$\hat{G}(s) = \frac{n(s)}{d(s)}$ ; pole = roots of  $d(s)$ ; zero =  $-n(s)$   
 $\hat{G}(s)$  is proper if  $\lim_{\omega \rightarrow \infty} \hat{G}(j\omega)$  is finite  
 $\Leftrightarrow \deg(d) \geq \deg(n)$

strictly proper  $\hat{G}(j\omega) = 0$

$$\Leftrightarrow \deg(d) > \deg(n)$$

biproper  $\hat{G}(s) \neq 0$  &  $\hat{G}^{-1}(s)$  are proper

$$\Leftrightarrow \deg(d) = \deg(n)$$

stable if analytic in the closed RHP

$$\Leftrightarrow \text{No RHP poles}$$

Theorem: 2-norm of rational  $\hat{G}(s)$  is finite iff

$\hat{G}$  is strictly proper, with no poles on  $Im$  axis.

... oo-norm  $\rightarrow$  proper, with  $\infty$

Induced Norm of system: (system gain)

$$\|G\| = \sup_{\|u\|_2=1} \|y\|_2 \quad \text{where } y = G * u$$

	$\ u\ _2$	$\ u\ _{\infty}$
$\ y\ _2$	$\ \hat{G}\ _2$	$\infty$
$\ y\ _{\infty}$	$\ \hat{G}\ _{\infty}$	$\ \hat{G}\ _1$

Need to show that  
 " = " = " > " + " < "

$\hat{G}$  stable & strictly proper

①  $\sup_{\|u\|_2 \leq 1} \|y\|_2 = \|\hat{G}\|_{\infty}$

proof: "  $\leq$  "  $\|y\|_2^2 = \|\hat{Y}(s)\|_2^2 = \|\hat{G}(s)\hat{U}(s)\|_2^2 = \frac{1}{2\pi} \int_{-\infty}^{\infty} |\hat{G}(j\omega)|^2 |\hat{U}(j\omega)|^2 d\omega$   
 $\leq \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{\sup_{\omega} |\hat{G}(j\omega)|^2 |\hat{U}(j\omega)|^2}{\|\hat{G}\|_{\infty}^2} d\omega = \|\hat{G}\|_{\infty}^2 \|\hat{U}\|_2^2 = \|\hat{G}\|_{\infty}^2 \|u\|_2^2$   
 ...  $\|y\|_2^2 \leq \|\hat{G}\|_{\infty}^2 \|u\|_2^2$

"  $\geq$  ": Find a "u" s.t.  $\|y\|_2 = \|\hat{G}\|_{\infty} \Rightarrow \sup(\cdot) \geq \|\hat{G}\|_{\infty}$

$$|\hat{U}_{\epsilon}(j\omega)| = \begin{cases} \sqrt{\frac{\epsilon}{\|\hat{G}\|_{\infty}}} & \omega_0 - \epsilon \leq \omega \leq \omega_0 + \epsilon \\ 0 & \text{o.w.} \end{cases}$$

where  $\|\hat{G}\|_{\infty} = \|\hat{G}(j\omega_0)\|$

$$\|u_{\epsilon}\|_2^2 = \|\hat{U}_{\epsilon}(s)\|_2^2 = 1$$

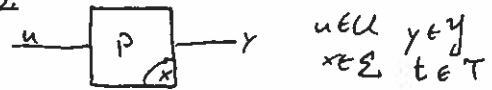
$$\|\hat{Y}_{\epsilon}(s)\|_2^2 = \frac{1}{2\pi} \int_{\omega_0 - \epsilon}^{\omega_0 + \epsilon} |\hat{G}(j\omega)|^2 \left(\sqrt{\frac{\epsilon}{\|\hat{G}\|_{\infty}}}\right)^2 d\omega \quad (\lim_{\epsilon \rightarrow 0})$$

$$= \frac{1}{2\pi} \int_{\omega_0 - \epsilon}^{\omega_0 + \epsilon} |\hat{G}(j\omega_0)|^2 \frac{\epsilon}{\|\hat{G}\|_{\infty}^2} d\omega$$

$$= \|\hat{G}\|_{\infty}^2 \frac{\epsilon}{2\pi} \int_{\omega_0 - \epsilon}^{\omega_0 + \epsilon} \frac{1}{\|\hat{G}\|_{\infty}^2} d\omega$$

$$= \|\hat{G}\|_{\infty}^2 \|u_{\epsilon}\|_2^2$$

10/7 L3:



$$y(t) = p(t, t_0, x_0, u(\cdot))$$

$$= r(t, s(t, t_0, x_0, u(\cdot)), u(t))$$

$$= r(t, s(t, t_0, x_0, 0), 0) + r(t, s(t, t_0, 0, u(\cdot)), u(t))$$

if linear  $\left\{ \begin{array}{l} \text{linear w.r.t. } x_0 \\ \text{linear w.r.t. } u(\cdot) \end{array} \right.$

$$= \text{zero-input response} + \text{zero-state response}$$

$$\|P\|_{2,2} = \sup_{\|u\|_2 \leq 1} \|y\|_2$$

Linear, state space, I/O differential equations

$$\frac{dx}{dt} = f(x, u, t) \quad y = h(x, t)$$

$$x \in \mathbb{R}^n = \mathcal{X}; \quad f: \mathbb{R}^n \times \mathbb{R}^m \times T \rightarrow \mathbb{R}^n; \quad h: \mathbb{R}^n \times T \rightarrow \mathbb{R}^p$$

Linear Systems:

$$\frac{dx}{dt} = A(t)x + B(t)u(t); \quad y = C(t)x$$

$\rightarrow$  Linear, time varying (non-autonomous) differential equations

$$A(t) \in \mathbb{R}^{n \times n}; \quad B(t) \in \mathbb{R}^{n \times m}; \quad C(t) \in \mathbb{R}^{p \times n}$$

$\rightarrow$  Linear, time invariant (LTI) I/O system

$$\dot{x} = Ax + Bu; \quad y = Cx$$

$\rightarrow$  Even more specific:  $u=0; \dot{x}=Ax; y=Cx$

$$x(t) = e^{A(t-t_0)} x_0 = s(t, t_0, x_0, 0)$$

$$y(t) = Ce^{A(t-t_0)} x_0 = p(t, t_0, x_0, 0)$$

Matrix Exponential:  $X \in \mathbb{R}^{n \times n}; e^X \in \mathbb{R}^{n \times n}$

$$e^X = I + X + \frac{1}{2}X^2 + \frac{1}{3!}X^3 + \dots$$

Ex:  $A = \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix}$   $\begin{cases} \dot{x}_1 = -x_1 \\ \dot{x}_2 = -2x_2 \end{cases} \rightarrow \begin{cases} x_1(t) = e^{-(t-t_0)} x_1(t_0) \\ x_2(t) = e^{-2(t-t_0)} x_2(t_0) \end{cases}$

$$\therefore e^{A(t-t_0)} = \begin{bmatrix} e^{-(t-t_0)} & 0 \\ 0 & e^{-2(t-t_0)} \end{bmatrix} \quad t_0=0$$

$$= \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} + \begin{bmatrix} -t & 0 \\ 0 & -2t \end{bmatrix} + \frac{1}{2} \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix}^2 t^2 + \dots$$

Ex:  $A = \begin{bmatrix} a & -b \\ b & a \end{bmatrix}$   $e^{At} = e^{at} \begin{bmatrix} \cos bt & -\sin bt \\ \sin bt & \cos bt \end{bmatrix}$

General:

Transforming Coordinates:

$$\dot{x} = Ax; \quad z = Tx; \quad T \in \mathbb{R}^{n \times n} \text{ (invertible)}$$

$$\dot{z} = T\dot{x} = TAx = TAT^{-1}z$$

$$z(t) = e^{(TAT^{-1})t} z(t_0)$$

$$e^{(TAT^{-1})t} = I + (TAT^{-1})t + \frac{1}{2}(TAT^{-1})^2 t^2 + \frac{1}{3!}(TAT^{-1})^3 t^3 + \dots$$

$$= I + (TAT^{-1})t + \frac{1}{2}(TAT^{-1})(TAT^{-1})t^2 + \dots$$

$$= I + (TAT^{-1})t + \frac{1}{2}TA^2T^{-1}t^2 + \frac{1}{3!}TA^3T^{-1}t^3$$

$$= T(I + At + \frac{1}{2}A^2t^2 + \frac{1}{3!}A^3t^3 + \dots)T^{-1}$$

$$\therefore e^{(TAT^{-1})t} = T e^{At} T^{-1}$$

$$\therefore e^{At} = T^{-1} e^{(TAT^{-1})t} T$$

$\sim$  Suppose we find T s.t.  $TAT^{-1}$  is easy to calculate

Ex: Diagonalizable matrix

Ex: Jordan form

$$J = \begin{bmatrix} J_1 & & 0 \\ & \ddots & \\ 0 & & J_k \end{bmatrix} \quad J_i = \begin{bmatrix} \lambda_i & 1 & & 0 \\ & \lambda_i & \ddots & \\ & & \ddots & 1 \\ 0 & & & \lambda_i \end{bmatrix}$$

Ex:  $\begin{bmatrix} -1 & 1 & 0 & 1 & 0 & 0 \\ 0 & -1 & 1 & 0 & 1 & 0 \\ 0 & 0 & -2 & 1 & 0 & 0 \\ 0 & 0 & 0 & -1 & 1 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 2 \end{bmatrix}$

10/7 L3 cont'd:

$$e^J = \begin{bmatrix} e^{\lambda_1} & & 0 \\ & \ddots & \\ 0 & & e^{\lambda_N} \end{bmatrix} \quad \begin{bmatrix} \lambda_1 & 0 \\ & \ddots \\ 0 & \lambda_k \end{bmatrix} = \begin{bmatrix} \lambda_1 & 0 \\ & \ddots \\ 0 & \lambda_k \end{bmatrix} + \begin{bmatrix} S_k & \\ & N_k \end{bmatrix}$$

Note:  $S_N = N_S$

$$e^{A+B} = I + (A+B) + \frac{1}{2}(A+B)^2 + \dots$$

$$= I + A+B + \frac{1}{2}(A^2+AB+BA+B^2) + \dots$$

$$+ \frac{1}{2}(A^2+2AB+B^2) + \dots$$

...  $e^{A+B} = e^A e^B$  \*Good to do on own

$$\therefore e^{J_k} = e^{S_k} e^{N_k} = \begin{bmatrix} e^{\lambda_k} & 0 \\ 0 & e^{\lambda_k} \end{bmatrix} \left( I + N_k + \frac{1}{2}N_k^2 + \dots + \frac{1}{(m_k-1)!} N_k^{m_k-1} \right)$$

$$N_k = \begin{bmatrix} 0 & 1 & & 0 \\ & 0 & \ddots & \\ & & \ddots & 1 \\ 0 & & & 0 \end{bmatrix}; N_k^2 = \begin{bmatrix} 0 & 0 & 1 & \\ & 0 & 0 & \ddots \\ & & 0 & 0 & \ddots \\ 0 & & & & 0 \end{bmatrix}$$

$$e^{J_k t} = \begin{bmatrix} e^{\lambda_k t} & t e^{\lambda_k t} & \dots & \frac{t^{m_k-1}}{(m_k-1)!} e^{\lambda_k t} \\ & e^{\lambda_k t} & & \\ & & \ddots & \\ 0 & & & e^{\lambda_k t} \end{bmatrix}$$

Theorem:  $\forall$  matrix  $A \in \mathbb{R}^{n \times n}$   $\exists$   $T \in \mathbb{R}^{n \times n}$  s.t.  $TAT^{-1}$  is in Jordan form

Claim: Sol'n for  $\dot{x} = Ax$ ,  $x(0) = x_0$ .  
 $x(t) = e^{At} x(0) \rightarrow e^{At} = T^{-1} e^{Jt} T$

Proof:  $\frac{dx}{dt} = \frac{d}{dt} \left( I + At + \frac{1}{2}A^2t^2 + \frac{1}{3!}A^3t^3 + \dots \right) x(0)$   
 $0 + A + A^2t + \frac{1}{2}A^3t^2 + \dots$   
 $= A(I + At + \dots) x_0 = A e^{At} x_0$

$$y(t) = r(t, \underbrace{s(t, t_0, x_0, 0)}_{C e^{A(t-t_0)} x_0}, 0) + r(t, s(t, t_0, 0, u(\cdot)), u(t))?$$

Claim: If  $x(0) = 0$  then  $x(t) = \int_0^t e^{A(t-\tau)} B u(\tau) d\tau$   
 $y(t) = \int_0^t C e^{A(t-\tau)} B u(\tau) d\tau$   
 ~Proof in notes.

Complex version of Jordan form:

$$J_k = \begin{bmatrix} a_k & -b_k & 0 & 0 \\ b_k & a_k & 0 & 0 \\ 0 & & \ddots & 0 \\ 0 & 0 & & a_k & -b_k \\ & & & b_k & a_k \end{bmatrix}$$

$\lambda_k = a_k + i b_k$  if  $A$  has complex eigenvalues.

Time varying systems:  $\Phi(t, t_0) = e^{A(t-t_0)}$   
 $y(t) = C \Phi(t, t_0) x(t_0) + \int_{t_0}^t C \Phi(t, \tau) B u(\tau) d\tau$

$\Phi(t, t_0)$  is the fundamental matrix  
 $\frac{\partial}{\partial t} \Phi(t, t_0) = A \Phi(t, t_0)$   $\Phi(t_0, t_0) = I$

10/a L4: Stability

I/O bounds:  $\|y\|_2 \leq \|G\| \|u\|_2$   
 I/O "stability": bounded input  $\Rightarrow$  bounded output  
 $\dot{x} = Ax \rightarrow x(t) = e^{At} x(0)$   
 If all eigenvalues  $\lambda_k$  of  $A$  have  $\text{Re}(\lambda_k) < 0$   
 $\Rightarrow e^{At} x(0) \rightarrow 0$  as  $t \rightarrow \infty$

Invariant Subspaces:

Definition: A subspace  $V \subset \mathbb{R}^n$  of dim  $k \leq n$  is  $A$ -invariant if  $AV \subset V$  and is  $e^{At}$ -invariant if  $e^{At} V \subset V \forall t$ .

Claim: All  $A$ -invariant subspaces are  $e^{At}$ -invariant  
 What are the  $A$ -invariant subspaces for any  $A$ ?

- Any eigenvector  $v$  defines an  $A$  invariant subspace  $\mathbb{C} \text{span}\{v\}$
- Any  $V = \text{span}\{v_1, \dots, v_p\}$  where  $v_i$  is a  $\lambda$ -vector  
 $A(\alpha_1 v_1 + \dots + \alpha_p v_p) = \alpha_1 A v_1 + \dots + \alpha_p A v_p$   
 $\rightarrow A = T J T^{-1}$   $V_{jk}$  is  $J$ -inv

$$T V_{jk} = \text{span}\{T v_{j,1}, \dots, T v_{j,m_j}\}$$

$$A(T V_{jk}) = T J T^{-1} T \cdot V_{jk} = T J V_{jk} \subset V_{jk}$$

take block elements of jordan form

Special invariant subspaces

$E^s = \mathbb{R}$  subspace corresponding to all "stable" eigenvalues  $\text{Re}(\lambda_k) < 0$   
 Ex: invariant  $J = \begin{bmatrix} -1 & & & \\ & -1 & & \\ & & -2 & \\ & & & 0 & \\ & & & & 0 & \\ & & & & & & 3 \end{bmatrix}$   $\lambda(T J T^{-1}) = \lambda(J)$

$$E^s = \text{span} \left\{ \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}, \begin{bmatrix} 0 \\ 1 \\ 0 \\ 0 \\ 0 \end{bmatrix}, \begin{bmatrix} 0 \\ 0 \\ 1 \\ 0 \\ 0 \end{bmatrix} \right\}$$

$E^u =$  subspace corresponding to  $\text{Re}(\lambda) > 0$   
 $E^c =$   $-e -$   $\text{Re}(\lambda) = 0$  ~ (c stands for centered)  
 $x(0) = X_0^s + X_0^u + X_0^c \rightarrow$  all orthogonal subspaces b/c of jordan form

$$X(t) = \underbrace{e^{At} X_0^s}_{\in E^s \rightarrow 0} + \underbrace{e^{At} X_0^u}_{\in E^u \rightarrow \infty} + \underbrace{e^{At} X_0^c}_{\text{not } \rightarrow \infty \text{ may be unbounded}}$$

ex:  $x = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \rightarrow e^{At} = \begin{bmatrix} 1 & t \\ 0 & 1 \end{bmatrix} \rightarrow$  unbounded

10/9 L4 cont'd:

More generally: Autonomous nonlinear diff eq.

$$\dot{x} = f(x)$$

Eq pt  $x_e$  is any point for which  $f(x_e) = 0$

$$e^{At} x_0 = 0 \rightarrow \dot{x} = Ax \rightarrow Ax_e = 0$$

↳ Null space of A

An eq. pt.  $x_e$  is stable if for any  $\epsilon \exists \delta$  s.t. for any  $x_0$  satisfying  $\|x(0) - x_e\| < \delta \Rightarrow \|x(t) - x_e\| < \epsilon$

start near  $\Rightarrow$  stay near

An eq. pt.  $x_e$  is asymptotically stable if it is stable and  $\|x(t) - x_e\| \rightarrow 0$  as  $t \rightarrow \infty$

Linear system  $\dot{x} = Ax$  is always an eq. pt.

Asypt. stable  $\Leftrightarrow \text{Re}(\lambda) < 0 \forall \lambda$  evals of A

~~stable if  $\text{Re}(\lambda) < 0$~~

Must be careful with non-trivial Jordan blocks

Eq. pt. is exponentially stable if  $\exists$  constants

$\alpha, \beta, m, M > 0$  s.t. (assuming  $x_e = 0$  w/o loss of generality)

$$\|x(t)\| \leq M e^{-\alpha t} \|x(0)\| \leq M e^{-\alpha t} \|x_0\|$$

↳ most negative eigenvalue

↳ can't converge faster for linear system

If  $\text{Re}(\lambda) < 0$  & trivial Jordan blocks then  $\alpha = \min \text{Re}(\lambda_i) < 0$

$$\beta = \max \text{Re}(\lambda_i) < 0$$

↳ envelope of decay  $\rightarrow$  can overshoot within bounds.

Linear: BIBO stable  $\Leftrightarrow$  exponentially stable

Steady-state response  $\rightarrow$  step response

$$p(t, t_0, x_0, u(\cdot)) = p(t, t_0, 0, u(\cdot)) + p(t, t_0, x_0, 0)$$

$$y(t) = C e^{A(t-t_0)} x_0 + \int_{t_0}^t C e^{A(t-\tau)} B u(\tau) d\tau + D u(t)$$

force response transience no steady state

$x(0) = 0$

$$y(t) = \int_0^t C e^{A(t-\tau)} B u(\tau) d\tau + D u(t) \rightarrow \text{step response.}$$

$$= C \left( \int_0^t e^{A(t-\tau)} B d\tau \right) u + D u$$

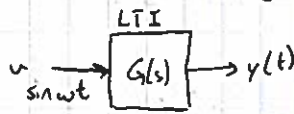
$$= C A^{-1} (e^{At} - I) B + D u$$

$$y(t) = \underbrace{(C A^{-1} e^{At} B)}_{\text{transience}} + \underbrace{(D - C A^{-1} B)}_{\text{steady state}} u$$

transience steady state

$\rightarrow$  can do same thing for impulse response

Ex:



$$\dot{x} = Ax + Bu$$

$$y = Cx + Du$$

$$\lambda = \text{eig}(A)$$

$$x(0) = 0$$

$\omega \gg |\lambda|$

start with  $u = e^{st}$

$$y(t) = C \int_0^t e^{A(t-\tau)} B e^{s\tau} d\tau$$

$$= C \int_0^t e^{(sI-A)(t-\tau)} B e^{s\tau} d\tau$$

$$= C e^{At} (sI-A)^{-1} (e^{(sI-A)t} - I) B$$

$$= C (sI-A)^{-1} B e^{st} - C (sI-A)^{-1} e^{At} B$$

$$s = j\omega \quad \omega \gg |\lambda(A)|$$

$$(j\omega I - A)^{-1} \approx -j\omega^{-1} I$$

$$y(t) = G(j\omega) e^{j\omega t} - C (j\omega I - A)^{-1} e^{At} B$$

$$\approx G(j\omega) e^{j\omega t} + \frac{j}{\omega} h(t) \quad h(t) \text{ is impulse response}$$

$$\approx \cos(\omega t) + \frac{j}{\omega} (\cos(\omega t) + j \sin(\omega t))$$

$$y(t) = \text{Im}(\dots)$$

$$y(t) = |G(j\omega)| \sin(\omega t + \arg(G(j\omega))) + \frac{1}{\omega} h(t)$$

10/11 Recitation. Coordinate Transformations

$\dot{x} = Ax + Bu$  } is this unique?  $\exists (A, B, C, D)$  where

$y = Cx + Du$  } behavior is identical?

$x \in \mathbb{R}^n, T \in \mathbb{R}^{n \times n}$  invertible

$$z = Tx \rightarrow x = T^{-1}z$$

$$\dot{z} = T \dot{x} = T(Ax + Bu)$$

$$\dot{z} = \underbrace{(TAT^{-1})}_{\hat{A}} z + \underbrace{TB}_{\hat{B}} u = \hat{A}z + \hat{B}u = \hat{z}$$

$$y = \underbrace{CT}_{\hat{C}} z + Du = \hat{C}z + Du$$

Linear systems are coordinate transform invariant.

$\therefore A$  and  $\hat{A}$  have identical Eigenvalues/vectors

$\rightarrow$  Poles are identical

To show this:  $Av = \lambda v ; \hat{A}\hat{v} = \lambda\hat{v}$

$$(TAT^{-1})\hat{v} = \lambda\hat{v}$$

$$A(T^{-1}\hat{v}) = \lambda(T^{-1}\hat{v}) \rightarrow \lambda(A) = \lambda(\hat{A})$$

$$x(t) = e^{At} x_0 + \int_0^t e^{A(t-\tau)} B u(\tau) d\tau$$

$$z(t) = e^{\hat{A}t} z_0 + \int_0^t e^{\hat{A}(t-\tau)} \hat{B} u(\tau) d\tau$$

$$z = Tx \quad \hat{A} = TAT^{-1} \quad \hat{B} = TB \quad z_0 = Tx_0$$

$$\star e^{T^{-1}AT} = T e^{AT} T^{-1}$$

$$z(t) = e^{(TAT^{-1})t} z_0 + \int_0^t e^{TAT^{-1}(t-\tau)} TB u(\tau) d\tau$$

$$= T e^{At} z_0 + \int_0^t e^{A(t-\tau)} B u(\tau) d\tau$$

$$z(t) = T x(t)$$

10/14 LS:

$$y(t) = C e^{At} x(0) + \int_0^t C e^{A(t-\tau)} B u(\tau) d\tau$$

$$\text{stability} \Leftrightarrow \lambda(A) \rightarrow E^s, E^u, E^c.$$



Can we choose  $u[0, T]$  s.t. if  $x(0) = x_0$  then  $x(T) = x_f \rightarrow$  given

$$x_0 \rightsquigarrow x_f$$

Reachability  $\rightarrow$



$$\dot{x} = f(x, u) \quad x(0) = x_0$$

$$u = \alpha(x)$$

Q: Is  $\dot{x} = f(x, \alpha(x))$  stable?

Stabilizability  $\rightarrow$

General concepts:  $D = \{u, \Sigma, y, s, r\}$

Definition: The state  $x_f \in \Sigma$  is reachable from  $x_0 \in \Sigma$  in time  $T > 0$  if  $\exists u \in \mathcal{U}[0, T]$  s.t.  $x(t) = x_f$  ( $x_0 \neq x_f$  is fine)

Reachable set in some time

$$R_{\Sigma}(x_0, \Sigma, T) = \{x(T) : u \in \mathcal{U}[0, T], x(0) = x_0 \text{ and } T \leq T\}$$

Definition: A system  $D$  is small-time locally controllable (STLC)

at  $x_0$  if for every  $T > 0 \exists \epsilon > 0 R(x_0, \Sigma, T) \supset B_{\epsilon}(x_0) = \{x : \|x - x_0\| < \epsilon\}$

Ex: Reachable:

STLC

$$R(x_0, \Sigma, T)$$



10/4 LS cont'd:

Linear System:  $\dot{x} = Ax + Bu$   $x \in \mathbb{R}^n, u \in \mathbb{R}^m$

To check reachability, look at range of linear map

$$\mathcal{L}_T: \mathcal{U} \rightarrow \mathbb{R}^n \rightsquigarrow \mathcal{L}_T(u(\cdot)) = \int_0^T e^{A(T-\tau)} Bu(\tau) d\tau$$

Don't include  $e^{At}$  so  $\forall c \rightarrow \int_0^T e^{A(T-\tau)} Bu(\tau) d\tau$

can be represented as constant offset (drift) on  $x_f$

$$L: \mathbb{R}^q \rightarrow \mathbb{R}^n \quad q > n \quad ; \quad x_f = Lu$$

$$x_f = \boxed{L} u \quad \text{need rank } L = n$$

$$u = L^T(LL^T)^{-1} x_f$$

Least squares  $u$ , can also have  $u$  in null space

Instead of  $L^T$  write  $L^*$  (adjoint matrix  $\rightarrow$  in

finite dimensions  $L^* = L^T$ )

$$(L^* w)(t) = \begin{cases} B^T e^{A^T(T-t)} w & \text{if } t \leq T \\ 0 & \text{if } t > T \end{cases}$$

Condition: need  $\text{rank} = \dim(\text{range } \mathcal{L}_T) = n$

$$\text{Claim: } \dim(\text{range } \mathcal{L}_T) = \dim \text{range}(\mathcal{L}_T^* \mathcal{L}_T)$$

$$\mathcal{L}_T^* \mathcal{L}_T = \int_0^T e^{A(T-\tau)} B B^T e^{A(T-\tau)} d\tau$$

$$[\text{Controllability Gramian for time } T] = \int_0^T e^{A\tau} B B^T e^{A^T\tau} d\tau = W_c(T)$$

~~Thm: A linear system is reachable~~

Given  $x_0 = 0$  &  $x_f$  claim that

$$u(t) = B^T e^{A^T(T-t)} W_c^{-1}(T) x_f$$

steers  $0 \rightarrow x_f$ .

Claim 1: If  $W_c(T)$  has rank  $n$ , we can go  $\forall w$  any two points in time  $T$  (Proof: plug in)

Claim 2: The dimension of the range ("rank") of  $W_c(T)$  is independent of  $T > 0$

Proof: (sketch) Suppose not full rank

$$\text{Then } \exists v \in \mathbb{R}^n \text{ s.t. } v^T W_c(T) = 0$$

$$\int_0^T v^T e^{A\tau} B B^T e^{A^T\tau} d\tau = 0$$

$\hookrightarrow v$  can go on either side. Will make it zero for all time.  $\therefore$  Reachability is time independent

If  $A$  is stable then let  $T \rightarrow \infty$ .

$$\text{Define } W_c = \lim_{T \rightarrow \infty} W_c(T) = \int_0^\infty e^{A\tau} B B^T e^{A^T\tau} d\tau$$

Theorem: A linear system is reachable iff  $W_c > 0$

Cor: Linear system is STLC iff  $W_c > 0$

Even Better!

$$1) AW_c + W_c A^T = -BB^T$$

$$2) \|G\|_2 = \|G\|_2 = \sqrt{CW_c C^T}$$

$2 \text{ norm} \rightarrow \infty$  norm gain

10/16 LG:

$$W_c(T) = \int_0^T e^{A\tau} B B^T e^{A^T\tau} d\tau$$

$$u(t) = B^T e^{A^T(T-t)} W_c^{-1}(T) x_f$$

Theorem: An LTI system is reachable (for any  $x_0, x_f, T$ ) and STLC iff any of the following hold:

(1)  $W_c(t) > 0$  for any  $T > 0$

(2)  $W_c$  satisfying  $AW_c + W_c A^T = -BB^T$  satisfies  $W_c > 0$  (and  $W_c = \lim_{T \rightarrow \infty} W_c(T)$  for  $A$  stable)

(3)  $\text{rank} [sI - A | B] \downarrow^n = n \quad \forall s \in \mathbb{C}$   
 $\leftarrow n+m \rightarrow$        $\rightarrow$  really only need to check  $s = \lambda(A)$

(4)  $\text{rank} [B | AB | A^2 B | \dots | A^{n-1} B] = n$

Proof: (#2  $\rightarrow$  rest in lecture notes)

$$AW_c + W_c A^T = A \int_0^T e^{A\tau} B B^T e^{A^T\tau} d\tau + \int_0^T e^{A\tau} B B^T e^{A^T\tau} d\tau A^T$$

$$= \int_0^T \frac{d}{d\tau} (e^{A\tau} B B^T e^{A^T\tau}) d\tau$$

$$= (e^{A\tau} B B^T e^{A^T\tau}) \Big|_0^T = -BB^T$$

Suppose that  $W_c$  is not full rank

$$\Rightarrow \exists v \text{ s.t. } v^T W_c v = 0$$

$v$  represents an unreachable direction

$$v^T e^{A\tau} B B^T e^{A^T\tau} v = 0 \Rightarrow v^T e^{A\tau} B = 0 \quad \forall \tau$$

$$\Rightarrow \int_0^t e^{A(t-\tau)} B u(\tau) d\tau \rightarrow \text{zero when projected onto } v.$$

$\hookrightarrow$  also true at  $\tau = 0 \rightarrow \therefore v^T B = 0$

$$\text{also } \frac{d}{d\tau} (v^T e^{A\tau} B) = v^T A e^{A\tau} B = 0 \Rightarrow v^T A B = 0$$

$\hookrightarrow$  leads to #4

#3) PBH test  $\rightarrow$  dropped rank means

$$v^T [sI - A] = 0 \rightarrow v^T B = 0$$

$$v^T (sI - A) = 0$$

$v^T$  must be a left eigenvector of  $A$  (e.v. of  $A^T$ )

On all tests: If we drop rank on any above test.

(E) we are trying to find directions you can't go.

Reachable space (from origin)  $\mathcal{R}(0, \leq T)$

= largest  $A$  invariant subspace containing  $B$

$$v^T W_c = 0, \quad v^T \text{ unreachable}$$

$$\mathcal{R} = \{w : v^T w = 0\}$$

Stability:  $\dot{x} = Ax + Bu \quad u = -kx$  ( $A|B$ ) is stabilizable

want  $\dot{x} = (A - Bk)x$  asy stable  $\text{Re}(\lambda(A - Bk)) < 0$

Stronger condition: given desired eigenvalues

$$\lambda_1^d, \dots, \lambda_n^d \text{ find } k \text{ s.t. } \lambda(A - Bk) = \{\lambda_1^d, \dots, \lambda_n^d\}$$

$\leftarrow$  Eigenvalue (Pole) placement  $\iff$  STLC

To prove, find  $T$  s.t.

$$T^T A T = \begin{bmatrix} -a_1 & -a_2 & \dots & -a_n \\ & & & 0 \\ & & & \vdots \\ & & & 0 \\ 0 & & & & -1 & 0 \end{bmatrix} \quad T^T B = \begin{bmatrix} 1 \\ 0 \\ \vdots \\ 0 \end{bmatrix}$$

if system is reachable such a  $T$  exists. (FBS 2c)

$$\det(SI - A) = s^n + a_1 s^{n-1} + a_2 s^{n-2} + \dots + a_{n-1} s + a_n$$

$$(A - Bk) = \begin{bmatrix} -a_1 & -a_2 & \dots & -a_n \\ 1 & 0 & \dots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 1 & \dots & 0 \end{bmatrix} - \begin{bmatrix} 1 \\ 0 \\ \vdots \\ 0 \end{bmatrix} [k_1, k_2, \dots, k_n]$$

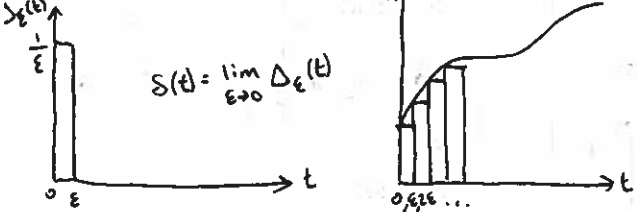
$$[u = -kx]$$

$$= \begin{bmatrix} -(a_1 + k_1) & -a_2 & \dots & -a_n \\ 1 & 0 & \dots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 1 & \dots & 0 \end{bmatrix} \leftarrow \text{roots of feedback char. poly.}$$

→ Pole placement.

10/8 Recitation:

Proof of convolution:



$$u(t) = \lim_{\epsilon \rightarrow 0} \sum_{i=0}^{\infty} u(i\epsilon) \epsilon \Delta_{\epsilon}(t - i\epsilon)$$

Impulse response  $h(t) = \lim_{\epsilon \rightarrow 0} y_{\epsilon}(t)$ ;  $y_{\epsilon}(t) = \int \Delta_{\epsilon}(t - i\epsilon) u(i\epsilon) \epsilon$

$$y(t) = \lim_{\epsilon \rightarrow 0} \left[ \sum_{i=0}^{\infty} u(i\epsilon) \epsilon y_{\epsilon}(t - i\epsilon) \right] = \int_0^{\infty} u(\tau) h(t - \tau) d\tau$$

21 L7: Optimal Control

Consider the system  $\dot{x} = f(x, u)$  with  $u \in U \subset \mathbb{R}^m$

Find  $u(\cdot)$  such that:

$$\min \int_0^T L(x(\tau), u(\tau)) d\tau + V(x(T))$$

s.t.  $\dot{x} = f(x, u)$   $x(0) = x_0$   $\Psi(x(T)) = 0$

$u \in U$   $\Psi = \begin{bmatrix} \psi_1(x) \\ \vdots \\ \psi_q(x) \end{bmatrix}$

$\Psi(x(T)) = 0$  ← final constraint

(e.g.  $\|x(T) - x_f\|^2 = \Psi(x(T))$ )

We will eventually specialize to

$$\dot{x} = Ax + Bu \quad u \in \mathbb{R}^m$$

$$J = \int_0^T (x^T Q x + u^T R u) d\tau + x^T(T) P x(T)$$

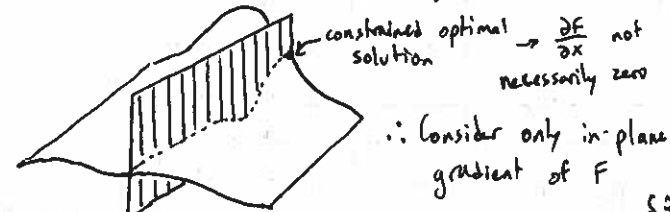
$Q \succ 0$   $R \succ 0$  (LQR)

Motivate/Review Static optimization

$F: \mathbb{R}^n \rightarrow \mathbb{R}$ , optimal input  $\rightarrow$  find  $x^*$  s.t.  $F(x^*) \geq F(x) \forall x \in \mathbb{R}^n$

Necessary condition:  $\frac{\partial F}{\partial x}(x^*) = 0$

Optimization with constraints:  $\rightarrow$  subject to  $G(x) = 0$



$$\frac{\partial F}{\partial x} + \sum \lambda_i \frac{\partial G_i}{\partial x} = 0 \text{ for some } \lambda \in \mathbb{R}^k$$

Special Cases:

- LQR
- $T = \infty$ : infinite horizon (drop  $V(x(T))$  &  $\Psi(x(T))$ )
- Constrained U

Define: Hamiltonian  $H: \mathbb{R}^n \times \mathbb{R}^m \times \mathbb{R}^n \rightarrow \mathbb{R}$

$$H(x, u, \lambda) = L(x, u) + \lambda^T f(x, u) = L(x, u) + \sum \lambda_i f_i(x, u)$$

Theorem: Maximum Principle: If  $(x^*, u^*)$  is optimal, then

- $\exists \lambda^*(t) \in \mathbb{R}^n$  and  $v^* \in \mathbb{R}^n$
- $\dot{x}^* = \frac{\partial H}{\partial x}(x^*, u^*, \lambda^*)$   $x(0)$  given  $\Psi(x^*(T)) = 0$
  - $\dot{\lambda}^* = -\frac{\partial H}{\partial \lambda}(x^*, u^*, \lambda^*)$   $\lambda^*(T) = \frac{\partial V}{\partial x}(x^*(T)) + v^T \frac{\partial \Psi}{\partial x}$
- and  $(a) H(x^*(t), u^*(t), \lambda^*(t)) \leq H(x^*(t), u, \lambda^*(t)) \forall u \in U$   $\rightarrow \Omega$  in notes

Structure:

- $\frac{\partial H}{\partial u} = f(x, u)$   $x \in \mathbb{R}^n$
- $\lambda \in \mathbb{R}^n$  Just an ODE with terminal condition
- Find  $u^* \in \mathbb{R}^m$  s.t. if  $\Omega \subset \mathbb{R}^m$  then a necessary condition is  $\frac{\partial H}{\partial u}(x^*, u^*, \lambda^*) = 0$

Finding optimal trajectories:

Step 1: Given  $x, \lambda$ , find minimum  $u$  where  $u = u(x, \lambda)$

Step 2: Solve the two-point boundary value problem

$$\dot{x} = f(x, u(x, \lambda)) \quad x(0) = x_0$$

$$\dot{\lambda} = -\frac{\partial H}{\partial \lambda}(x, u(x, \lambda), \lambda) \quad \lambda(T) = \text{something} \left[ \frac{\partial V}{\partial x}(x(T)) + v^T \frac{\partial \Psi}{\partial x} \right]$$

Suppose  $L(x, u) = x^T Q x + u^T R u$   $R \succ 0$

$$\Psi(x(T)) = x^T P x \quad \dot{x} = Ax + Bu$$

$$\dot{x} = Ax + Bu \rightarrow \dot{x} = Ax - BR^{-1} B^T \lambda \quad x(0) = x_0$$

$$\dot{\lambda} = -Qx + A^T \lambda \quad \lambda(T) = P x(T) \frac{B^T \lambda}{R}$$

$$0 = \frac{\partial H}{\partial u} = Ru + \lambda^T B \rightarrow u = -R^{-1} \lambda^T B$$

Let's guess that  $\lambda(t) = P(t)x(t)$

plug into  $\dot{\lambda} \rightarrow -\dot{P}x - PAx + PBR^{-1}B^T Px = Qx + A^T Px$

$$-\dot{P} = PA + A^T P - PBR^{-1}B^T P + Q \rightarrow P(T) = P_1$$

Strategy:

- Solve PLA by reverse integrating
  - set  $\lambda(t) = P(t)x(t)$
  - solve  $\dot{x} = Ax - BR^{-1}B^T P(t)x$   $x(0) = x_0$  by integrating forward in time.
- Riccati ODE

23 L8:

From before  $u^* = \text{argmin}_u H(x, u, \lambda) \rightarrow u(t) = -R^{-1} B^T P(t) x$

Remarks: 1) can change from "steering" to origin to steering to  $x_f$  eq pt.

$$z = x - x_f; \dot{z} = Ax + Bu = A(z + x_f) + Bz = Az + Bu$$

2) Control is in the form of feedback law

3) If  $T = \infty$  and  $P_1 = 0$  then if  $\exists$  a constant P satisfying

$$0 = PA + A^T P - PBR^{-1}B^T P + Q \leftarrow \text{algebraic Riccati equation (ARE)}$$

[If (A, B) is reachable then P > 0 satisfying A.R.E. always exists]

$\rightarrow$  then  $u = -R^{-1} B^T P x$  is optimal

Recall  $\min F(x)$  s.t.  $G_i(x) = 0$

$$\tilde{J}(x, u, \lambda) = J(x, u) + \int_0^T -\lambda^T (f(x(t)) - f(x, u)) dt + v^T \Psi(x(T))$$

$$= \int_0^T (L(x, u) - \lambda^T (f(x(t)) - f(x, u))) dt + V(x(T)) + v^T \Psi(x(T))$$

$$\tilde{J}(x(t), u(t), \lambda(t)) = \int_0^t (H(x, u) - \lambda^T \dot{x}) dt + V(x(t)) + v^T \Psi(x(t))$$

$$\delta \tilde{J} = \int_0^T \left( \frac{\partial H}{\partial x} \delta x + \frac{\partial H}{\partial u} \delta u - \lambda^T \delta \dot{x} \right) dt + \frac{\partial V}{\partial x} \delta x(T) + v^T \frac{\partial \Psi}{\partial x} \delta x(T) + \delta v^T \Psi(x(T), u(T))$$

Integration by parts:  $-\int_0^T \lambda^T \delta \dot{x} dt = -\lambda^T(T) \delta x(T) + \lambda^T(0) \delta x(0) + \int_0^T \dot{\lambda}^T \delta x dt$

0/23 L8 cont'd:

Maximum principle:

$$\dot{x} = f(x, u) \quad x(0) = x_0 \quad u \in \Omega$$

$$J(x, u) = \int_0^T L(x, u) dt + V(x(T)) \rightarrow \min J(x, u) \text{ s.t. } \psi(x(T)) = 0$$

$$H(x, u, \lambda) = L(x, u) + \lambda^T f(x, u)$$

optimal solution:

$$\dot{x} = \frac{\partial H}{\partial x}(x, u, \lambda) \quad x(0) = x_0$$

$$-\dot{\lambda} = \frac{\partial H}{\partial x}(x, u, \lambda) \quad \lambda(T) = \frac{\partial V}{\partial x}(x(T)) + \lambda^T \frac{\partial \psi}{\partial x}$$

$$u^* = \operatorname{argmin}_u H(x, u, \lambda) \quad ; \quad \frac{\partial H}{\partial u}(x, u^*, \lambda) = 0$$

All we are doing is  $\min f(x)$  s.t.  $G_i(x) = 0$   
 $\tilde{F} = F + \lambda^T G, \quad \frac{\partial \tilde{F}}{\partial x} = 0$  for  $n$  dimensional spaces

Choosing Cost Function:

Most Common:  $Q = I; R = PI$

$$J = \int_0^{\infty} (\|x\|^2 + \rho \|u\|^2) dt$$

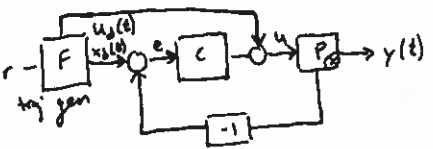
$\rho$  trades error for energy

Next most common:

$$Q = \begin{bmatrix} q_{11} & & & \\ & \ddots & & \\ & & 0 & \\ & & & q_{nn} \end{bmatrix} \quad R = \begin{bmatrix} r_{11} & & & \\ & \ddots & & \\ & & 0 & \\ & & & r_{nn} \end{bmatrix}$$

$$J = \int_0^{\infty} (q_{11}x_1^2 + q_{22}x_2^2 + \dots + q_{nn}x_n^2 + u^T R u) dt$$

Two degree-of-freedom design (for NL systems):



$$\begin{aligned} \dot{x} &= f(x, u) & L \text{ can be } f(x_d, u_d) \\ \dot{x}_d &= f(x_d, u_d) \\ e &= f(x, u) - f(x_d, u_d) = f(x_d + e, u_d + v) - f(x_d, u_d) \\ &= F(e, v, x_d, u_d) \approx A(x_d, u_d)e + B(x_d, u_d)v \end{aligned}$$

10/25 Recitation: Discrete Time LQR

$x_{k+1} = Ax_k + Bu_k$ ;  $x_0$  given

LQR (Objective Function)

$$J(U) = \sum_{t=0}^{N-1} (x_t^T Q x_t + u_t^T R u_t) + x_N^T Q_f x_N \quad ; \quad U = (u_0, u_1, \dots, u_{N-1})$$

$$Q = Q^T \geq 0, \quad Q_f = Q_f^T \geq 0, \quad R = R^T > 0$$

Aside:  $u = L_f^{-1} (L_f L_f^{-1})^T x_f$  minimizes  $\|u\|_{L^2}$

Least Squares Solution:

$$\begin{bmatrix} x_0 \\ x_1 \\ \vdots \\ x_N \end{bmatrix} = \begin{bmatrix} 0 & B & 0 & \dots & 0 \\ AB & B & & & \\ \vdots & \vdots & \ddots & & \\ AN^2B & \dots & B & & \end{bmatrix} \begin{bmatrix} u_0 \\ u_1 \\ \vdots \\ u_{N-1} \end{bmatrix} + \begin{bmatrix} I \\ A \\ \vdots \\ A^N \end{bmatrix} x_0$$

$$X = G \cdot U + H x_0$$

$$\text{cost: } J(U) = \left\| \operatorname{diag}(Q^0, \dots, Q^{N-1}, Q_f) (GU + Hx_0) \right\|^2 + \left\| \operatorname{diag}(R^0, \dots, R^{N-1}) U \right\|^2$$

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$$\begin{aligned} \text{DP: } J_t^*(U) &= \sum_{\tau=t}^{N-1} (x_\tau^T Q x_\tau + u_\tau^T R u_\tau) + x_N^T Q_f x_N \\ (t=N) &= (x_N^T Q_f x_N + u_N^T R u_N) + \sum_{\tau=t+1}^{N-1} (x_\tau^T Q x_\tau + u_\tau^T R u_\tau) + x_N^T Q_f x_N \\ &= J_{t+1}(U_{t+1}) \end{aligned}$$

Define value function:  $V_t(x_t) = \min_{u_t} J_t(U_t)$

$$= \min_{u_t \in \Omega} \sum_{\tau=t}^{N-1} (x_\tau^T Q x_\tau + u_\tau^T R u_\tau) + x_N^T Q_f x_N$$

Ansatz:  $V_k(z) = z^T P_k z$

$$\text{s.t. } x_k = x_k^0$$

$$x_{\tau+1} = Ax_\tau + B u_\tau, \quad \tau = t, \dots, N-1$$

Proof:

$$\textcircled{1} \text{ Base: } t=N; \quad J_N(z) = x_N^T Q_f x_N \Rightarrow P_N = Q_f$$

$$V_N(z) = \min_u J_N(z) = z^T Q_f z$$

$\textcircled{2}$  Induction: Assume  $V_{k+1}(z) = z^T P_{k+1} z$

$$V_k(z) = \min_{u_k, \dots, u_{N-1}} \sum_{\tau=k}^{N-1} (x_\tau^T Q x_\tau + u_\tau^T R u_\tau) + x_N^T Q_f x_N$$

$$= \min_{u_k} \left\{ x_k^T Q x_k + u_k^T R u_k + \min_{u_{k+1}, \dots, u_{N-1}} \left\{ \sum_{\tau=k+1}^{N-1} (\dots) + x_N^T Q_f x_N \right\} \right\}$$

$$= \min_{u_k} \left\{ x_k^T Q x_k + u_k^T R u_k + x_{k+1}^T P_{k+1} x_{k+1} \right\}$$

$$x_{k+1} = Ax_k + Bu_k = Az + Bu_k$$

$$= \min_{u_k} \left\{ u_k^T (R + B^T P_{k+1} B) u_k + 2u_k^T B^T P_{k+1} A z + z^T (Q + A^T P_{k+1} A) z \right\}$$

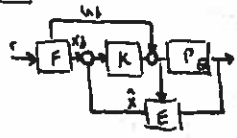
$$\frac{\partial V_k}{\partial u_k} = 0 \Rightarrow u_k^* = -(R + B^T P_{k+1} B)^{-1} B^T P_{k+1} A x_k$$

$$V_k(z) = x_k^T \underbrace{[Q + A^T P_{k+1} A - A^T P_{k+1} B (R + B^T P_{k+1} B)^{-1} B^T P_{k+1} A]}_{P_k} x_k$$

Procedure:

- $\textcircled{1}$  Set  $P_N = Q_f$
- $\textcircled{2}$  For  $t=N, \dots, 1$   $P_{t-1} = Q + A^T P_t A - A^T P_t B (R + B^T P_t B)^{-1} B^T P_t A$
- $\textcircled{3}$  For  $t=0, \dots, N-1$   $K_t = -(R + B^T P_{t+1} B)^{-1} B^T P_{t+1} A$
- $\textcircled{4}$  For  $t=0, \dots, N-1$  optimal  $u_t^* = K_t x_t$

10/28 L9:



Estimator:  $\dot{\hat{x}} = f(\hat{x}, u) \quad x \in \mathbb{R}^n \quad u \in \mathbb{R}^m$   
 $y = h(\hat{x}) \quad y \in \mathbb{R}^p$

$$\frac{d\hat{x}}{dt} = \underbrace{f(\hat{x}, u)}_{\text{prediction}} + \alpha \underbrace{(y - h(\hat{x}))}_{\text{correction}}$$

Q1: When can we determine  $x(t)$  from  $y[0, \epsilon], u[0, \epsilon]$

Distinguishability:  $\mathcal{D} = (U, \Sigma, Y, S, r)$

$$I/O \text{ map: } p(t, x_0, t_0, u(\cdot)) = r(t, s(t, x_0, t_0, u), u)$$

Definition: A dynamical system  $\mathcal{D}$  is distinguishable on  $[t_1, t_2]$  if  $\forall x_0 \neq z_0 \exists u(\cdot)$  s.t.  $p(t, x_0, t_0, u(\cdot)) \neq p(t, z_0, t_0, u(\cdot))$  for some  $t \in [t_1, t_2]$

Definition: A dynamical system  $\mathcal{D}$  is observable on  $[t_1, t_2]$  if every  $u(\cdot)$  initial state  $x_0$  is distinguishable for every  $z_0 \neq x_0$ .  $\mathcal{D}$  is observable if it is observable on any  $[t_1, t_2]$ . An observer is a mapping  $\mathcal{O}: U \times Y \rightarrow \Sigma$  that returns  $x_0$  given  $u(\cdot)$  &  $y(\cdot)$ .

$$p(t, x_0, t_0, u(\cdot)) = C e^{A(t-t_0)} x_0 + \int_{t_0}^t C e^{A(t-\tau)} B u(\tau) d\tau$$

$$p: \Sigma \times U \rightarrow Y$$

If  $u(\cdot) \neq 0$  then choose  $\hat{y} = y - \int_{t_0}^t \dots \therefore$  W/o loss assume  $d) = 0$

$$M_T(x_0)(t) = Ce^{At} x_0 \quad \begin{bmatrix} M \\ \end{bmatrix} \begin{bmatrix} x \\ \end{bmatrix} = \begin{bmatrix} y \\ \end{bmatrix} \quad x = (MTM)^{-1} MTy$$

$$M_T: \Sigma \rightarrow \mathcal{Y}$$

$$M_T^* \sigma = \int_0^T e^{A^T \tau} C^T \sigma(\tau) d\tau$$

$$(M_T^* M_T) = \int_0^T e^{A^T \tau} C^T C e^{A \tau} d\tau$$

Wol(T) → observability Gramian

(A, B) is observable iff Wol(T) is full rank (n) and

$$x_0 = (W_0(T))^{-1} \int_0^T e^{A^T \tau} C^T y(\tau) d\tau$$

If (A, C) is not observable then  $\exists v \neq 0 \in \mathbb{R}^n$  s.t.  $W_0 v = 0$  and all  $x_0 = \alpha v$  w/  $\alpha \in \mathbb{R}$  generate identical outputs (0)

Can show:  $W_0(T) > 0$  doesn't depend on T

If A is stable, define  $W_0 := \lim_{T \rightarrow \infty} W_0(T)$  and  $W_0$  satisfies  $A^T W_0 + W_0 A = -C^T C$

A pair (A, C) is observable iff the following conditions hold:

- 1)  $W_0(T) > 0$  for some (or any)  $T > 0$
- 2) If A is stable, solution of  $A^T W_0 + W_0 A = -C^T C$  is pos. def. ( $W_0 =$  observability Gramian)
- 3) PBH:  $\text{rank} \begin{bmatrix} C \\ sI - A \end{bmatrix} = n \quad \forall s \in \mathbb{C} (s \in \lambda(A))$
- 4) Observability rank test  $\text{rank} \begin{bmatrix} C \\ CA \\ \vdots \\ CA^{n-1} \end{bmatrix} = n$

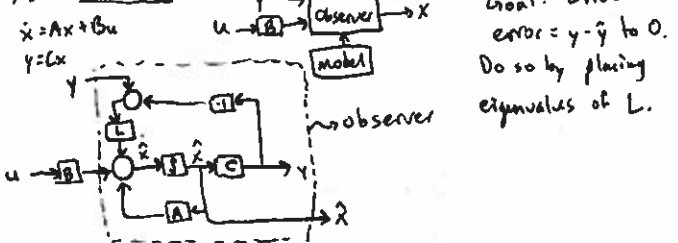
Estimators: "Observer"  $u, y \rightarrow \hat{x}$   
"Estimator"  $u, y \rightarrow \hat{x}(t)$

$$\begin{aligned} \dot{\hat{x}} &= A\hat{x} + Bu & y &= Cx \\ \dot{\hat{x}} &= A\hat{x} + Bu + L(y - C\hat{x}) & e &= \hat{x} - x \\ \dot{e} &= Ae - LCe = (A - LC)e & e(0) &= \hat{x}(0) - x(0) \end{aligned}$$

If  $\text{Re} \lambda(A - LC) < 0$  then  $e \rightarrow 0$  as  $t \rightarrow \infty$

Q: When can we assign  $\lambda$ s to arbitrary values?

o/so Recitation:



Goal: Drive error =  $y - \hat{y}$  to 0. Do so by placing eigenvalues of L.

In the above diagram  $u \rightarrow [B] \rightarrow [F] \rightarrow [K] \rightarrow y$

observer based controller design

$$\hat{u} = -k\hat{x} \rightarrow u = r + \hat{u}$$

$$\begin{aligned} \dot{\hat{x}} &= A\hat{x} + Bu + L(y - \hat{y}) & y &= Cx & \hat{y} &= C\hat{x} \\ \Rightarrow \dot{\hat{x}} &= A\hat{x} + Bu + LC(x - \hat{x}) & \dot{x} &= Ax + Bu \end{aligned}$$

$$\tilde{x} = x - \hat{x} \quad \dot{\tilde{x}} = \dot{x} - \dot{\hat{x}}$$

$$\dot{\tilde{x}} = A\tilde{x} - LC(x - \hat{x}) = (A - LC)\tilde{x} = \tilde{\dot{x}}$$

Observer based state feedback controller:  $u = -k\hat{x} + k_f r$

$$\dot{x} = Ax + B(-k\hat{x} + k_f r) \quad \text{w/ } \hat{x} = x - \tilde{x}$$

$$\dot{x} = (A - Bk)x + Bk_f r + Bk\tilde{x}$$

$$\text{Now consider } \begin{bmatrix} \dot{\tilde{x}} \\ \dot{x} \end{bmatrix} = \begin{bmatrix} A - Bk & Bk \\ 0 & A - LC \end{bmatrix} \begin{bmatrix} \tilde{x} \\ x \end{bmatrix} + \begin{bmatrix} Bk_f \\ 0 \end{bmatrix} r$$

Separation principle: you can design the controller and observer independently.

- System should be reachable & controllable. If so you can arbitrarily place the eigenvalues of k & L independently.

Example:  $\dot{x} = \begin{bmatrix} -4 & 1 \\ -6 & 1 \end{bmatrix} x + \begin{bmatrix} 3 \\ 7 \end{bmatrix} u$   $\det(sI - A) = s^2 + 3s + 2$   
 $a_1 = 3, a_2 = 2$

$$y = [1 \quad -1]x$$

$$W_0 = \begin{bmatrix} C \\ CA \end{bmatrix} = \begin{bmatrix} 1 & -1 \\ 2 & 0 \end{bmatrix} \quad \tilde{W}_0 = \begin{bmatrix} 1 & 0 \\ -a_1 & 1 \end{bmatrix}$$

↳ full rank  $\therefore \exists T$  to  $\tilde{x}, \tilde{A}, \tilde{B}$

$$T = \tilde{W}_0^{-1} W_0 = \begin{bmatrix} 1 & 1 \\ 5 & -3 \end{bmatrix}$$

$$\tilde{A} = TAT^{-1} = \begin{bmatrix} -3 & 1 \\ -2 & 0 \end{bmatrix} \quad \tilde{B} = TB = \begin{bmatrix} -4 \\ -6 \end{bmatrix} \quad \tilde{C} = CT^{-1} = [1 \quad 0]$$

1/1 L10: Linear I/O system  $\dot{x} = Ax + Bu$   $x(0) = x_0$   $u \in \mathbb{R}^m$   
Summary:  $y = Cx$   $x \in \mathbb{R}^n$   $y \in \mathbb{R}^l$

$$y(t) = Ce^{At} x_0 + \int_0^t Ce^{A(t-\tau)} Bu(\tau) d\tau$$

Reachability:  $\mathcal{R} = \text{range}(W_r) = \int_0^T e^{A(T-\tau)} Bu(\tau) d\tau$

$$W_r(T) = \int_0^T e^{A\tau} BB^T e^{A^T \tau} d\tau$$

$$AW_r + W_r A^T = -BB^T \quad W_r = \lim_{T \rightarrow \infty} W_r(T)$$

$$u(t) = B^T e^{A^T(T-t)} W_r^{-1}(t) x_f$$

Reachable set = range  $W_r$

Observability:  $M_T(x_0) = Ce^{AT} x_0$

$$W_0(T) = \int_0^T e^{A^T \tau} C^T C e^{A \tau} d\tau$$

$$A^T W_0 + W_0 A = -C^T C$$

$$x_0 = (W_0(T))^{-1} \int_0^T e^{A^T \tau} C^T y(\tau) d\tau$$

$\dot{x} = Ax + Bu, y = Cx$  what if not reachable and/or not observable?

Kalman Decomposition:  $\mathbb{R}^n = E_{r0} \oplus E_{r\bar{0}} \oplus E_{\bar{r}0} \oplus E_{\bar{r}\bar{0}}$

$$\begin{aligned} E_r &= E_{r0} \oplus E_{r\bar{0}} = \text{range } W_r \\ E_{\bar{r}\bar{0}} &= E_{\bar{r}0} \oplus E_{\bar{r}\bar{0}} = \text{null } W_0 \end{aligned} \quad \text{Note: both are A-invariant}$$

$E_{r\bar{0}} = \text{range } W_r \cap \text{null } W_0 \leftarrow A$ -invariant  
 $E_{r0} = \text{space such that } E_r = E_{r0} \oplus E_{r\bar{0}} \leftarrow$  not necessarily A-invariant  
↑ not unique, anything to complete space

$E_{\bar{r}0} = \text{space such that } E_{\bar{r}\bar{0}} = E_{\bar{r}0} \oplus E_{\bar{r}\bar{0}}$   
 $E_{\bar{r}\bar{0}} = \dots$  completes  $\mathbb{R}^n$

Theorem: Given A, B, C,  $\exists$  coordinates  $z = Tx$  s.t. in z-coords

$$\tilde{A} = \begin{bmatrix} A_{r0} & 0 & * & 0 \\ * & A_{r\bar{0}} & * & * \\ 0 & 0 & A_{\bar{r}0} & 0 \\ 0 & 0 & * & A_{\bar{r}\bar{0}} \end{bmatrix} \quad \tilde{B} = \begin{bmatrix} B_{r0} \\ B_{r\bar{0}} \\ B_{\bar{r}0} \\ 0 \end{bmatrix} \quad \tilde{C} = [C_{r0} \quad 0 \quad C_{\bar{r}0} \quad 0]$$

Balanced Representation:

Can show  $\exists T$  s.t.

$$\tilde{W}_c = \tilde{W}_o = \begin{bmatrix} \sigma_1 & & 0 \\ & \ddots & \\ 0 & & \sigma_n \end{bmatrix} \quad |z| = T \leq \sigma_1 > \sigma_2 > \dots > \sigma_n > 0$$

$$\tilde{W}_c \tilde{W}_o = \begin{bmatrix} \sigma_1^2 & & 0 \\ & \ddots & \\ 0 & & \sigma_n^2 \end{bmatrix} \leftarrow \text{don't care about these}$$



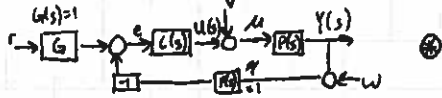
1/3 L10 cont'd:

Suppose that we drop the last  $k$  states in the balanced representation.

$$\|G - \hat{G}\|_{\infty} \leq 2 \sum_{i=1}^{k-1} \sigma_i \text{ "twice the sum of tails"}$$

1/4 L11: FREQUENCY DOMAIN

$$U(s) = \int_0^{\infty} u(t)e^{-st} dt$$



State space  $\rightarrow$  Transfer functions

$$Y(s) = C(sI - A)^{-1}x(0) + C(sI - A)^{-1}BU(s)$$

Initial Condition response TF:  $H(s)$   
 $H(s) = \frac{n(s)}{d(s)} = \frac{b_{k-1}s^{k-1} + \dots + b_1s + b_0}{s^n + a_{n-1}s^{n-1} + \dots + a_1s + a_0}$   
 $n(s) = 0 \Rightarrow$  zeros  
 $d(s) = 0 \Rightarrow$  poles

$n(s) = b_1 = CB, b_2 = CA^{k-1}B + \dots + a_1 CA^{k-1}B$   
 $d(s) = \det(sI - A)$  "Markov parameters"

There are many state space "realizations" of transfer functions

Ex:  $A = \begin{bmatrix} -a_1 & & & 0 \\ & -a_2 & & \\ & & \ddots & \\ & & & -a_n & & 0 \\ & & & & & 0 \end{bmatrix}$   $B = \begin{bmatrix} 1 \\ 0 \\ \vdots \\ 0 \end{bmatrix}$   $C = [b_1 \ b_2 \ \dots \ b_n]$

$u \rightarrow G_1 \rightarrow G_2 \rightarrow y \quad y = G_2 G_1 u$

$u \rightarrow G_1 \parallel G_2 \rightarrow y \quad y = (G_1 + G_2)u$

$u \rightarrow G_1 \rightarrow G_2 \rightarrow y \quad y = G_2 G_1 u$   
 $u \rightarrow G_1 \rightarrow G_2 \rightarrow y \quad y = (I + G_1 G_2)^{-1} G_1 u$

matrix of transfer functions

Properties: Stability, Performance, Robustness

Stability: I/O stability, BIBO stability

$H(s)$  is BIBO stable iff poles of  $H(s)$  are in open LHP

Definition: A feedback system is internally stable if all

I/O transfer functions are stable

$$\begin{bmatrix} e \\ u \\ y \end{bmatrix} = \begin{bmatrix} G & -P & -I \\ 1+PC & 1+PC & 1+PC \\ C & 1 & -C \\ 1+PC & 1+PC & 1+PC \\ PC & P & 1 \\ 1+PC & 1+PC & 1+PC \end{bmatrix} \begin{bmatrix} r \\ v \\ w \end{bmatrix} \rightarrow \text{assuming } f=1$$

Theorem:  $\odot$  is internally stable iff  $n_p n_c n_f + d_p d_c d_e$  has no RHP zeros (assuming  $G(s)$  is stable)

Proof: ( $f=1$ ) Sketch

$$\begin{bmatrix} e \\ u \\ y \end{bmatrix} = \frac{1}{n_p n_c + d_p d_c} \begin{bmatrix} d_p d_c & -n_p d_c & d_p d_e \\ d_p n_c & d_p d_c & d_p n_c \\ n_p n_c & n_p d_c & d_p d_e \end{bmatrix} \begin{bmatrix} r \\ v \\ w \end{bmatrix}$$

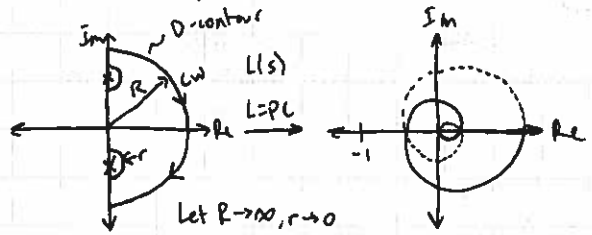
If  $(n_p n_c + d_p d_c)(s_0) = 0$  for  $\text{Re}(s_0) > 0$ , show that at least one of the xfer fns will be unstable. Need to show that so will not be in numerator for at least one of the 3 entries

★ CDS QUALS QUESTION

Theorem 2:  $\odot$  is internally stable iff the following two conditions hold:

- (1)  $1+PCF$  has no RHP zeros
- (2) No RHP pole/zero cancellations in PCF

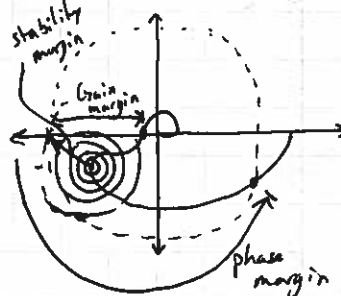
Theorem 3: Nyquist



$-1$  is special because of the  $1+PC$  condition.  
 # net CW encirclements =  $-\#$  unstable poles of  $P/L + \#$  unstable zeros of  $1+P$   
 $N = -P + Z$   
 can count  $\uparrow$  given  $\uparrow$  how many unstable  $\odot$  pole

MIMO: plot max singular value of  $L(s)$

Intuition of Nyquist



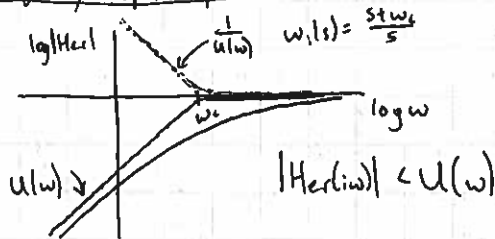
$-k$  Gain margin  
 $-e^{j\phi}$  phase margin

"How stable am I"

Performance

Asymptotic tracking: Given  $r(t)$  find controller  $C$  such that  $(P,C)$  is internally stable &  $\lim_{t \rightarrow \infty} (y(t) - r(t)) = 0$

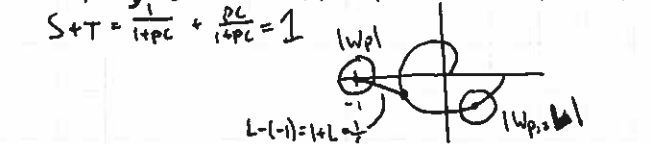
Frequency response profiles



Rewrite:  $\|W_p Herl\|_{\infty} < 1 \rightarrow$  Make  $W_p$  large in regions where you want small error:  $W_p = \frac{1}{U(w)}$

Choose  $W_p(s)$  such that  $|W_p(j\omega)| \approx \frac{1}{U(\omega)}$   
 $Her = \frac{1}{1+PC} =: S \rightarrow$  sensitivity function

$\|W_p S\|_{\infty} < 1$  weight sensitivity  
 $\|W_p P\|_{\infty} \|H_{gr}\|_{\infty} < 1$   $H_{gr} = \frac{PC}{1+PC} =: T \rightarrow$  complementary



1/8 Recitation: Nyquist:

Time Domain

$G: \dot{x} = Ax + Bu$

$y = Cx + Du$

Stability:  $\text{Re}(\text{eig}(A)) < 0$

$\det(\lambda I - A) = 0$

roots( $\det(\lambda I - A)$ )

Frequency Domain

$G(s)$

Stability:  $\text{Re}(\text{poles}(G(s))) < 0$

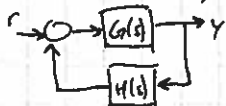
$G(s) = C(sI - A)^{-1}B + D$

poles( $G(s)$ )

roots( $\det(sI - A)$ )

Why use Nyquist?

- 1) Determine CL stability from OL information
- 2) Better understanding of structural aspects of stability
- 3) Geometric tool to visualize frequency response
- 4) Relative stability
- 5) Robust stability



OLTF:  $G(s)H(s)$

CLTF:  $\frac{G(s)}{1+G(s)H(s)}$

Nyquist Criterion:

$G(s) = \frac{N_G}{D_G}$

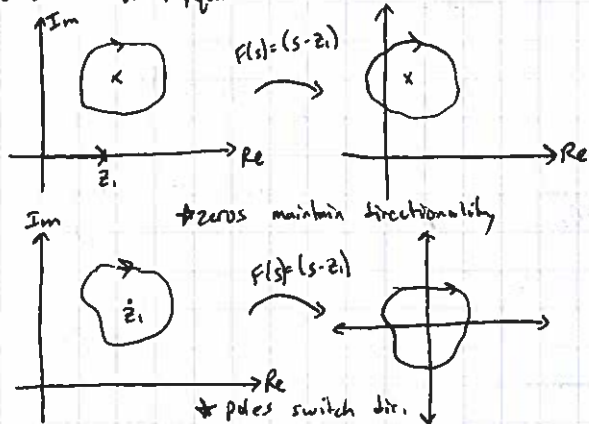
$H(s) = \frac{N_H}{D_H}$

$F(s) := \text{denominator of CLTF} = 1 + GH = 1 + \frac{N_G N_H}{D_G D_H}$

$= \frac{D_G D_H + N_G N_H}{D_G D_H} \rightarrow \text{poles}(CLTF)$

$\rightarrow \text{poles}(OLTF)$

Motivation for Nyquist:



zeros maintain directionality

poles switch dir.

If encircles the pole, it is shifted to origin

- Because  $OL = F(s) - 1$ , we map encirclements of poles to the value -1. This is why we care about encirclements of -1.
- Let  $e_z = \#$  encircled zeros,  $e_p = \#$  encircled poles
- if  $e_z = e_p$ : No encirclements of origin
- $e_z > e_p$ : Same direction
- $e_z < e_p$ : opposite direction

zeros & poles of  $F(s) - 1$

From  $\odot$ ,  $N = Z_p - P_p$

$\rightarrow$  cw # of encirclements of -1    # LTF RHP poles    # OLF RHP poles

$\therefore Z = N + P$

$\rightarrow$  cw w/c zeros maintain direction ( $\omega$ ) contour

Nyquist is just the complex plot of bode w/c

Bode is  $|L(j\omega)|$  for  $\omega = 0 \rightarrow \infty$ .

Ch 6:

- $h(t) = Ce^{At}B + D\delta(t)$
- $y(t) = Ce^{At}x_0 + \int_0^t h(t-\tau)u(\tau)d\tau$
- $e^{At} = I + At + \frac{1}{2}A^2t^2 + \dots = \sum_{k=0}^{\infty} \frac{1}{k!}A^k t^k$
- Consider the transformation to block Jordan form  
 $\tilde{A} = TAT^{-1}$ ,  $\tilde{B} = TB$ ,  $\tilde{C} = CT^{-1}$   
 Then because  $e^{TAT^{-1}t} = Te^{At}T^{-1}$ , we have  
 $x(t) = T^{-1}e^{\tilde{A}t}Tx(0) + T^{-1}\int_0^t e^{\tilde{A}(t-\tau)}\tilde{B}u(\tau)d\tau$
- $y(t) = \underbrace{CA^{-1}e^{At}B}_{\text{transient}} + \underbrace{D-CA^{-1}B}_{\text{steady-state}}$

Ch 7:

- $W_c(T) = \int_0^T e^{AT}BB^Te^{A^Tt}dt$
- $\tilde{x}(t) = B^Te^{A^T(T-t)}W_c^{-1}(T)x_f$
- Reachability tests:
  - 1)  $W_c(T) > 0$  for any  $T > 0$
  - 2)  $W_c$  satisfies  $AW_c + W_c^TA^T = -BB^T$  and  $W_c > 0$   
(and  $W_c = \lim_{T \rightarrow \infty} W_c(T)$  for  $A$  stable)
  - 3)  $\text{rank}[sI - A|B] = n \quad \forall s \in \mathbb{C}$
  - 4)  $\text{rank}[B|AB|A^2B|\dots|A^{n-1}B] = n$

• Reachable canonical form:

$$\tilde{A} = TAT^{-1} = \begin{bmatrix} -a_1 & -a_2 & -a_3 & \dots & -a_n \\ 1 & 0 & 0 & \dots & 0 \\ 0 & 1 & 0 & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & \dots & \dots & \dots & 1 \end{bmatrix} \quad \tilde{B} = T^{-1}B = \begin{bmatrix} 1 \\ 0 \\ \vdots \\ 0 \end{bmatrix}$$

$$CT = [b_1 \ b_2 \ \dots \ b_n] \quad T = \begin{bmatrix} T & W_r & W_c^{-1} \\ \hline \tilde{B} & \tilde{A} & \tilde{B}^{-1} \end{bmatrix} \rightarrow [B \ \tilde{A} \ B^{-1}]$$

• Stabilizability:

- Pole placement of  $(A - Bk)$
- LQR:  $J(x_0) = \int_0^{\infty} (x^T Q x + u^T Q_u u) dt + x^T(t_f) Q_f x(t_f)$
- Algebraic RE:  $0 = PA + AP - PBQ^{-1}B^T P + Q_x$   
 $\hookrightarrow u = -Q_u^{-1}B^T P x$  is optimal
- $Q_x > 0$ ;  $Q_u > 0$  to guarantee existence of solution  
 $\hookrightarrow Q_u > 0$  because it needs to be invertible. (for sol.)  
 $\hookrightarrow Q_x > 0$  so integral cost is zero iff  $x=0$   
 $\hookrightarrow$  can allow  $\geq 0$  if we don't care about some states

Ch 8:

- $W_o(T) = \int_0^T e^{AT} C^T C e^{A^T t} dt$   
 $x_0 = (W_o(T))^{-1} \int_0^T e^{A^T t} C^T y(t) dt$
- Observability tests:
  - 1)  $W_o(T) > 0$  for any  $T > 0$
  - 2) If  $A$  is stable, solution of  $ATW_o + W_oA^T = -C^T C$  is positive definite
  - 3) PBH:  $\text{rank}[sI - A] = n \quad \forall s \in \mathbb{C}$
  - 4)  $\text{rank} \begin{bmatrix} C \\ CA \\ \vdots \\ CA^{n-1} \end{bmatrix} = n$

• Observable canonical form:

$$\frac{dz}{dt} = \begin{bmatrix} -a_1 & 1 & & 0 \\ -a_2 & 0 & \dots & 0 \\ \vdots & \vdots & \ddots & 1 \\ -a_n & & & 0 \end{bmatrix} z + \begin{bmatrix} b_1 \\ b_2 \\ \vdots \\ b_n \end{bmatrix} u$$

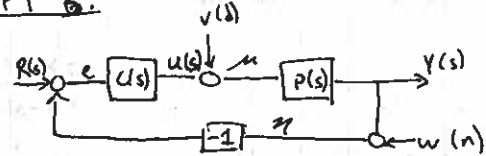
$T = W_o^{-1}W_0$

$y = [1 \ 0 \ \dots \ 0]z + b_0 u$

• Observer:  $\dot{\hat{x}} = A\hat{x} + Bu + L(y - C\hat{x})$   
 $\tilde{x} = x - \hat{x}$ ;  $\dot{\tilde{x}} = (A - LC)\tilde{x}$

• Observability: Pole placement of  $(A - LC)$

DFT B:



$$Y(s) = C(sI - A)^{-1}x_0 + C(sI - A)^{-1}B U(s)$$

$$\frac{b_1 s^{n-1} + \dots + b_n s + b_0}{s^n + a_1 s^{n-1} + \dots + a_n} = H(s) = \frac{\text{zeros}}{\text{poles}}$$

• Internally stable if all I/O tf are stable

$$\begin{bmatrix} e \\ u \end{bmatrix} = \frac{1}{1+PC} \begin{bmatrix} 1 & -P & -Z \\ C & 1 & -C \\ PC & P & 1 \end{bmatrix} \begin{bmatrix} r \\ v \\ w \end{bmatrix} \quad \begin{bmatrix} e \\ u \end{bmatrix} = - \begin{bmatrix} PS & S \\ T & CS \end{bmatrix} \begin{bmatrix} d \\ n \end{bmatrix}$$

• Internally stable iff:

- $1+PC$  has no zeros in  $\text{Re } s \geq 0$
- $PC$  has no pole/zero cancellations in  $\text{Re } s \geq 0$ .

• Nyquist:

# net CW encirclements = -# unstable poles of PC + # unstable zeros of  $1+PC$

DFT 4:  $S = \frac{1}{1+PC} = \text{Her}$ ;  $T = \frac{PC}{1+PC} = \text{Hyn}$

- Robust performance:  $W_p \in W_z$ ;  $W_r \in W_z$
- Robust stability: (Pg 56 DFT)

Perturbation	Condition	TYPE
$(1 + \Delta W_z)P$	$\ W_z T\ _{\infty} < 1$	Multiplicative
$P + \Delta W_z$	$\ W_z C S\ _{\infty} < 1$	Additive
$P / (1 + \Delta W_z P)$	$\ W_z P S\ _{\infty} < 1$	Feedback
$P / (1 + \Delta W_z)$	$\ W_z S\ _{\infty} < 1$	

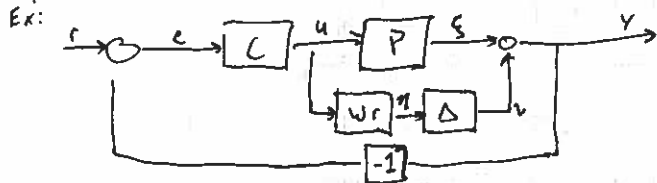
• Nominal performance condition  $\|W_i S\|_{\infty} < 1$

• Robust Performance:

Perturbation	Nominal Perf. Condition	
	$\ W_i S\ _{\infty} < 1$	$\ W_i T\ _{\infty} < 1$
$(1 + \Delta W_z)P$	$\ W_i S\  + \ W_z T\ _{\infty} < 1$	~
$P + W_z \Delta$	$\ W_i S\  + \ W_z C\ _{\infty} < 1$	~
$P / (1 + \Delta W_z P)$	~	$\ W_i T\  + \ W_z P S\ _{\infty} < 1$
$P / (1 + \Delta W_z)$	~	$\ W_i T\  + \ W_z S\ _{\infty} < 1$

• plug & chug to get  $\rightarrow$  (63 DFT)

Small Gain Theorem: If  $\|G\|_{\infty} < 1$  &  $\|H\|_{\infty} \leq 1$  and  $G$  &  $H$  are stable then the closed loop system is stable.



$$\begin{aligned} \eta &= W_r u ; u = Ce ; e = v - Pu \\ \Rightarrow u &= Ce = C(v - Pu) \Rightarrow u(P(1+C)) = Cv \Rightarrow u = \frac{C}{1+PC} v \\ \Rightarrow \eta &= W_r C S v \\ \therefore H &= W_r C S. \end{aligned}$$

How to get robust stability condition.

DFT 5:

$$\text{If } P \in S, C = \left\{ \frac{Q}{1-PQ} : Q \in S \right\}. \text{ If } P \notin S, C = \left\{ \frac{X+MQ}{Y-NQ} : Q \in S \right\}$$

Theorem 3:  $P$  is strongly stabilizable iff it has an even # of real poles between every pair of real zeros in  $\text{Re } s \geq 0$ .

DFT 6: Limits of performance

- check first for stability

Algebraic Limits: (always true)

- $S+T=1$
- $\min \{ |W_1(j\omega)|, |W_2(j\omega)| \} < 1 \quad \forall \omega$
- If  $p$  is a pole of  $L$  in  $\text{Re } s \geq 0$  &  $z$  is zero in  $\text{Re } s \geq 0$ :
 
$$\begin{aligned} S(p)=0 \quad S(z)=1 &\Rightarrow \|W_1 S\|_{\infty} \geq |W_1(z)| \\ T(p)=1 \quad T(z)=0 &\Rightarrow \|W_2 T\|_{\infty} \geq |W_2(p)| \end{aligned}$$

Maximum modulus principle: if stable & bounded (analytic),

max will occur on  $j\omega$  axis.

Bode's Integral formula:

$$\int_0^{\infty} \ln |S(j\omega)| d\omega = \pi \sum_{p_i \in \text{RHP (of } L)} p_i$$

All-pass TF:

$$\text{All pass: } H(s) \rightarrow |H(j\omega)| = 1 \quad \forall \omega.$$

Theorem:  $G(s) = G_{mp} \cdot G_{ap}$   
no RHP poles/zeros  $\rightarrow$  All pass

Ex (14.4 FBS pg 14)

$$P(s) = \frac{n(s)}{d(s)} \tilde{P}(s)$$

$$S(s) = \frac{1}{1+P(s)C(s)} = \frac{d(s)}{d(s)+n(s)\tilde{P}(s)C(s)} \cdot W_P = \frac{d(-s)}{d(s)}$$

$$M_S = \max_{\omega} |S(j\omega)| = \max |W_P(j\omega)S(j\omega)| \geq |W_P(z_R)S(z_R)| = \left| \frac{d(-z_R)}{d(z_R)} \right|$$

The waterbed effect:

Suppose  $P$  has a zero w/  $\text{Re } z > 0$ . Then  $\exists c_1, c_2$  as functions only on  $\omega_1, \omega_2, z$  such that

$$c_1 \log M_1 + c_2 \log M_2 \geq \log |Sap(z)|^{-1} \geq 0.$$

$$\text{where } M_1 := \max_{\omega_1 \leq \omega \leq \omega_2} |S(j\omega)| ; M_2 := \|S\|_{\infty}$$

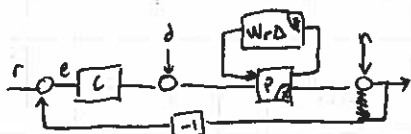
11 L13: Uncertainty & Robustness:

$$P \begin{cases} \dot{x} = f(x, u, \Delta, \theta, z) \\ y = h(x, \theta, \Delta) \end{cases} \quad \theta \in \Theta$$

- Q: When is the CL system stable  $\forall \theta \in \Theta$
- Q: When is performance satisfied - // -
- $\dot{z} = g(x, z, \theta)$  unmodeled dynamics  $g \in \mathcal{G}$
- In addition,  $\forall g \in \mathcal{G}$

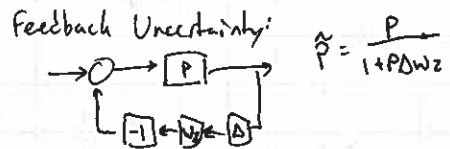
- $n, d$  exogenous inputs not affected by  $x, z$
- $z$  coupled dynamical uncertainty
- $\theta$  often constant approximation for dynamic quantity
- $\dot{\theta} = 0$  is a special case of  $\dot{z} = \dots$

Linear (Control) Systems:



Processes:  $P \in \mathcal{P} = \{ \tilde{P} : \|\Delta\|_{\infty} < 1 \}$   
 Robust stability  $\iff$  internally stable  $\forall P \in \mathcal{P}$   
 Performance  $\iff \|W_p S\|_{\infty} \leq 1 \quad \forall P \in \mathcal{P}$

Common types of uncertainty:  $\tilde{L} = \tilde{P}C$



Robust Stability:

Then (small gain) If  $\|G\|_{\infty} < 1$  &  $\|H\|_{\infty} \leq 1$  and  $G, H$  are stable then closed loop is stable



Feedback:  $H = -P W_r$   
 Multiplicative:  $H = \frac{W_r P C}{1 + P C} \rightarrow \|W_r T\|_{\infty} < 1$   
 Complementary sensitivity func  $L_s = \frac{P C}{1 + P C} = 1 - S$

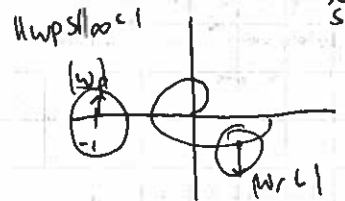
More generally: Assume  $W_r$  stable  
 Theorem:  $\tilde{P} = P(1 + W_r \Delta)$ ,  $\|\Delta\|_{\infty} < 1$  is internally stable  $\iff \|W_r T\|_{\infty} < 1$

Pract! (unstable open loop): key: look for changes of encirclements of -1  
 $1 + \tilde{P}C = 1 + PC(1 + W_r \Delta)$   
 $= (1 + PC)(1 + \frac{PC}{1 + PC} W_r \Delta)$

$$\|T W_r \Delta\|_{\infty} \leq \|W_r T\|_{\infty} \|\Delta\|_{\infty} < 1$$

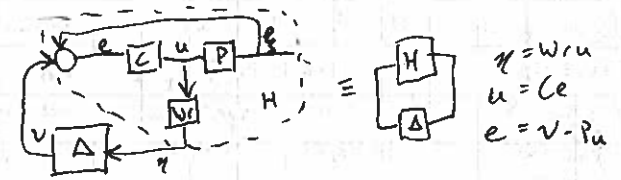
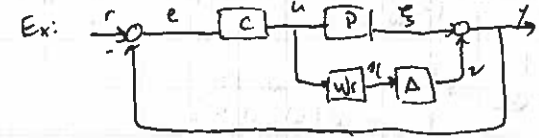
Robust Performance:

Performance criterion:  $\|W_p S\|_{\infty} \leq 1$   
 Robust performance  $\iff$  robust stability &  
 $\|W_p \tilde{S}\|_{\infty} \leq 1$   
 $\tilde{S} = \frac{1}{1 + \tilde{P}C} \quad \tilde{P} \in \dots$



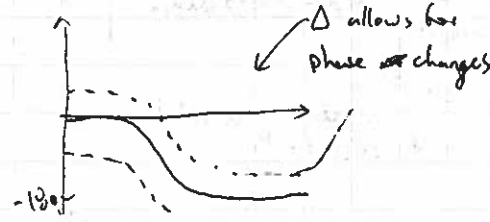
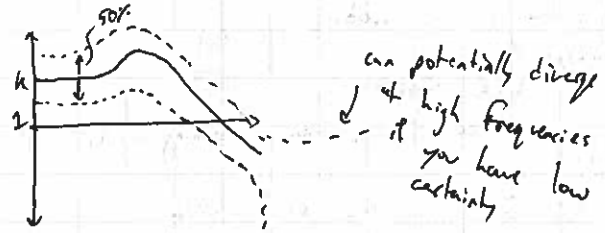
$$\|W_p S\|_{\infty} + \|W_r T\|_{\infty} < 1$$

13 L14:

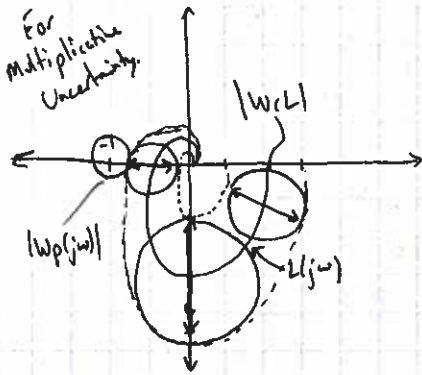


$$\rightarrow u = C e = C(v - P u) \rightarrow u(1 + P C) = C v \rightarrow u = \frac{C}{1 + P C} v$$

$\eta = W_r C S v$   
 Ex:  $P = \frac{k}{s^2 + 2\zeta\omega_n s + \omega_n^2}$   $k = k_{nom} \pm 50\%$   
 $\tilde{P} = P(1 + 0.5\Delta)$ ,  $\|\Delta\|_{\infty} \leq 1$ ,  $W_r = 0.5$



1/13 LHC cont'd.



Robust Performance:

Theorem 2: If  $P$  has multiplicative uncertainty with weight  $W_r$  and performance spec is  $\|W_p S\|_\infty < 1$  then the system has robust performance ( $W_p \tilde{S} \|_\infty < 1$ ,  $\tilde{S} = \frac{1}{1+PC}$ ,  $P \in \mathcal{P}(w,r)$ ) iff  $\|W_p S + W_r T\|_\infty < 1$   
nominal performance or robust stability

Acid:  $\sup_{\omega} |G| = \|G\|_\infty$  iff  $G$  is stable!  
 ∴ Roughly, we need to show (1) robust stability & (2)  $\|W_p \tilde{S}\|_\infty < 1$

$$\|W_p \tilde{S}\|_\infty = \left\| \frac{W_p}{1+PC} \right\|_\infty = \left\| \frac{W_p}{1+P(1+W_r \Delta)} \right\|_\infty \quad \forall \Delta$$

$$\frac{1}{1+PC(1+W_r \Delta)} = \frac{1}{1+PC} \frac{(1+PC)}{(1+PC)+PCW_r \Delta} = \frac{1}{1+W_r T \Delta}$$

$$\left| \frac{W_p S}{1-W_r T} \right| \geq \left| \frac{W_p S}{1+W_r T} \right| \quad \forall |\Delta| \leq 1 \text{ assuming } |w_r T| < 1$$

show this.

$$\frac{|W_p S|}{1-|w_r T|} < 1 \rightarrow |W_p S| < 1 - |w_r T|$$

$$|w_r T| + |W_p S| < 1 \quad \forall s \in j\omega$$

Perturbation	Stability	$\ W_p S\ _\infty < 1$	$\ W_r T\ _\infty < 1$
$P(1+W_r \Delta)$	$\ W_r T\ _\infty < 1$	$\ W_r T + W_p S\ _\infty < 1$ messy...	
$P W_r \Delta$	$\ W_r S\ _\infty < 1$	$\ W_p S + W_r T\ _\infty < 1$ messy...	
$P(1+W_r \Delta)$	$\ W_r S\ _\infty < 1$	messy...	$\ W_r S + W_p T\ _\infty < 1$

Recitation:

$$P_1 = \frac{1}{s+1} \quad P_2 = \frac{1}{s+a}$$

Show:  $P_1$  can be turned into  $P_2$  w/ bounded additive & multiplicative uncertainty if  $a > 0$  not if  $a < 0$ . Also, no restriction on  $a$  if feedback uncertainty is used.

Strategy:  $P_1$  = nominal system (P)  
 $P_2$  = perturbed (P)

Find allowable  $\Delta, W_2$  s.t. by tuning  $\Delta, P_1 \rightarrow P_2$

Additive:

$$\tilde{P} = \frac{1}{s+a} = P_1 + \Delta a W_a = \frac{1}{s+1} + \Delta a W_a$$

$$\Delta a W_a = \frac{1-a}{(s+1)(s+a)} \rightarrow d := 1-a \rightarrow \Delta a W_a = \frac{d}{(s+1)(s+1-d)}$$

$$\rightarrow P_1: d=0, P_2: d=1-a$$

$$\Delta a W_a \text{ bounded} \Leftrightarrow \frac{d}{(s+1)(s+1-d)} \text{ no RHP} \Leftrightarrow 1-d > 0 \Leftrightarrow a > 0$$

Multiplicative:

$$(1 + \Delta_m W_m) P_1 = P_2 \rightsquigarrow \Delta_m W_m = \frac{1-a}{s+1}$$

Feedback:

$$P_2 = P_1 / (1 + \Delta_m W_m) \rightsquigarrow \Delta_m W_m = a-1$$

$\Delta_m W_m$  bounded  $\Leftrightarrow$  no restriction on  $a$ .

\*Exercise:

$$P_1 = \frac{s+1}{(s+1)^2} \quad P_2 = \frac{s+a}{(s+1)^2}$$

Show: add + Mult. no restriction on a feedback:  $a > 0$ .

Theorem 2: Robust Performance  $\Leftrightarrow \|W_1 S + W_2 T\|_\infty < 1$

$$\rightsquigarrow \text{Robust performance} \begin{cases} \|W_2 T\|_\infty < 1 \\ \|W_1 \frac{S}{1+\Delta W_2 T}\|_\infty \leq 1 \quad \forall \text{ allowable } \Delta \end{cases}$$

$$W_1 S \Leftrightarrow \|W_1 S + W_2 T\|_\infty < 1$$

Proof:  $\|W_1 S + W_2 T\|_\infty < 1$

$$\hookrightarrow s = j\omega \quad \begin{cases} |W_2 T| < 1 \\ |W_1 S + W_2 T| < 1 \quad \forall \omega \end{cases}$$

$$\hookrightarrow \begin{cases} |W_2 T| < 1 \\ |W_1 S| - |W_2 T| < 1 \quad \forall \omega \end{cases}$$

$$\hookrightarrow \begin{cases} \|W_2 T\|_\infty < 1 \\ \|W_1 S / (1 - W_2 T)\|_\infty < 1 \end{cases}$$

$$\max_{|\Delta| < 1} \left\| \frac{W_1 S}{1 + \Delta W_2 T} \right\|_\infty = \left\| \frac{W_1 S}{1 + |W_2 T|} \right\|_\infty$$

$$\Leftrightarrow \max_{|\Delta| < 1} \max_{\omega} \left| \frac{W_1 S}{1 + \Delta W_2 T} \right| = \max_{\omega} \left| \frac{W_1 S}{1 - |W_2 T|} \right|$$

can switch these (LHS) (RHS)

2. Pick  $w_1$  s.t. max is achieved

$$\exists \Delta \text{ s.t. } |1 + \Delta W_2 T| = 1 - |W_2 T| \text{ at } w_2$$

$$\Leftrightarrow \max_{|\Delta| < 1} \left| \frac{W_1 S}{1 + \Delta W_2 T} \right| \geq \left| \frac{W_1 S}{1 - |W_2 T|} \right|$$

$$\leq \max_{w_1} \max_{|\Delta| < 1} \left| \frac{W_1 S}{1 + \Delta W_2 T} \right| \rightarrow \left\| \frac{W_1 S}{1 - |W_2 T|} \right\| \text{ RHS}$$

(LHS)

$$\leq \frac{|1 + \Delta W_2 T - \Delta W_2 T|}{|1 + \Delta W_2 T + \Delta W_2 T|} \leq |D| |W_2 T| \leq |W_2 T| \text{ if allowable}$$

$$\rightarrow \|1 + \Delta W_2 T\| \geq 1 - |W_2 T| \quad \forall \Delta$$

$$\frac{1}{|1 + \Delta W_2 T|} \leq \frac{1}{1 - |W_2 T|} \rightarrow \frac{|W_1 S|}{|1 + \Delta W_2 T|} \leq \frac{|W_1 S|}{1 - |W_2 T|} \quad \forall \omega$$

$$\left\| \frac{W_1 S}{1 + \Delta W_2 T} \right\|_\infty \leq \left\| \frac{W_1 S}{1 - |W_2 T|} \right\|_\infty \rightarrow \text{LHS} \leq \text{RHS} \quad \therefore = \square$$

1/18: Other types of questions:

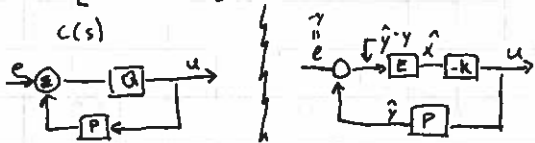
- Given  $P$ , what is the set of all controllers  $C$  that stabilize  $(P, C)$ ,  $C \in \mathcal{C}$ ?
- Given controller  $C$  that stabilizes some process  $P$ , what is the set of all  $P$  that  $C$  stabilizes.
- Given  $P$ , what are the fundamental limits of performance for any controller  $C$ ?

1. Let  $\mathcal{S} = \{P : P \text{ stable \& proper}\}$

Case 1: If  $P$  is stable, then  $C$  stabilizing  $\iff C = \frac{Q}{1+PQ}$   $Q \in \mathcal{S}$

Proof:  $Q = \frac{C}{1+PC} = CS$

$$\begin{bmatrix} S & CS \\ PS & T \end{bmatrix} = \begin{bmatrix} 1-PQ & Q \\ P(1-PQ) & PQ \end{bmatrix}$$



Case 2:  $P$  is unstable: need coprime factorization

$P = N_p M_p^{-1}$  (right coprime factorization)

$\tilde{M}_p^{-1} \tilde{N}_p$  (left coprime factorization)

$M_p, N_p \in \mathcal{S}$  with no common factors (p/z cancelling)

Easy coprime factorization

$$N_p = \frac{n(s)}{(s+\lambda)^n}; M_p = \frac{d(s)}{(s+\lambda)^n} \quad \frac{N_p}{M_p} = \frac{n}{d}$$

Theorem:  $N, M \in \mathcal{S}$  coprime

$$\exists X, Y \in \mathcal{S} \text{ s.t. } MX + NY = I$$

$\hookrightarrow$  intuition: generalization of Bezout's identity.

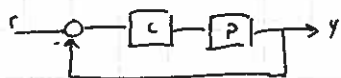
Theorem:  $C$  stabilizing  $\iff C = (X+MQ)/(Y-NQ)$   $Q \in \mathcal{S}$

$\hookrightarrow$  Youla-parameterization (Q-parameterization)

$$S = M(Y-NQ) \text{ affine in } Q$$

$$T = N(X+MQ)$$

1/20 Recitation: Coprime Factorization.



Recap:  $\mathcal{S}$ : family of all stable, proper, real, rational functions

Case 1: If  $p$  is stable:  $\exists C$  stabilizing

$$\iff C = \frac{Q}{1+PQ}, Q \in \mathcal{S}$$

Case 2: If  $P$  is unstable:  $\exists C$  stabilizing

$$\iff C = \frac{X+MQ}{Y-NQ}, Q \in \mathcal{S}$$

Right:  $\left\{ \begin{array}{l} P = NM^{-1} \\ MX + NY = I \end{array} \right\}$  (Youla Parameterization)

Left:  $\left\{ \begin{array}{l} P = M^{-1}N \\ MX + NY = I \end{array} \right\}$

Example:  $P = \frac{s^2+2s+1}{s^3+1} \frac{3a}{3b}$

$$s^2+2s+1 = \underbrace{(s^3+1)}_a \underbrace{(0)}_b + \underbrace{(s^2+2s+1)}_r$$

$$a = bq + r, \text{gcd}(a, b) = \text{gcd}(b, r) \dots = r \neq 0$$

Starting over:

$$s^2+2s+1 = (s^3+1)(0) + (s^2+2s+1)$$

$$(s^3+1) = (s^2+2s+1)(s-2) + (3s+3) \rightarrow \text{last nonzero remainder, } \therefore = \text{gcd.}$$

$$\hookrightarrow (s+1) = (s^2+2s+1)\left(\frac{2-s}{3}\right) + \left(\frac{s^2+1}{3}\right)$$

$$1 = \frac{s^2+2s+1}{s+1}\left(\frac{2-s}{3}\right) + \frac{s^2+1}{3(s+1)}$$

$\hookrightarrow$  Will not give us  $Q \in \mathcal{S}$ , we need something else  
 $\hookrightarrow$  Procedure B (DFT Ch.5).

$$\text{Map: } s = \frac{1-\lambda}{\lambda}, \lambda = \frac{1}{s+1}, \tilde{P}(\lambda) = \frac{n(\lambda)}{m(\lambda)} \rightarrow \text{GCD again}$$

$\rightarrow$  Do above again and it works out

$$P = \frac{s^2-s-2}{s^3-2s^2-3s}, s = \frac{1-\lambda}{\lambda}$$

$$\tilde{P} = \frac{\left(\frac{1-\lambda}{\lambda}\right)^2 - \left(\frac{1-\lambda}{\lambda}\right) - 2}{\left(\frac{1-\lambda}{\lambda}\right)^3 - 2\left(\frac{1-\lambda}{\lambda}\right)^2 - 3\left(\frac{1-\lambda}{\lambda}\right)} = \frac{\lambda - 4\lambda^2}{-6\lambda^3 + 4\lambda^2 + \lambda + 1} \frac{3a}{3b}$$

$$\text{Long Div: } (-6\lambda^3 + 4\lambda^2 + \lambda + 1) = (-4\lambda^2 + \lambda) \left(\frac{3}{2} - \frac{5}{8}\right) + \left(\frac{13}{8} + 1\right)$$

$$(-4\lambda^2 + \lambda) = \left(\frac{13}{8} + 1\right) \left(\frac{-32\lambda}{13} + \frac{36\lambda}{16}\right) + \left(\frac{-360}{16}\right) = r, \text{next step} = 0.$$

$$\hookrightarrow 1 = \left(\frac{16}{360} + \frac{5}{2} - \frac{5}{3}\right)(4\lambda^2 - \lambda) + \left(\frac{16}{360}\right)(-6\lambda^3 + 4\lambda^2 + \lambda + 1) \left(\frac{-32\lambda}{13} + \frac{36}{16}\right)$$

$\rightarrow$  convert back to  $s$  via  $\lambda = \frac{1}{s+1}, P = NM^{-1}$

$$C = \frac{X+MQ}{Y-NQ}, Q \in \mathcal{S}. \text{ this controller will stabilize } P.$$

State space form:  $P(s) = \begin{bmatrix} A & B \\ C & D \end{bmatrix} = C(sI - A)^{-1}B + D$

$$\begin{bmatrix} P_1 & P_2 \\ P_3 & P_4 \end{bmatrix} = \begin{bmatrix} A & B_1 & B_2 \\ c_1 & D_{11} & D_{12} \\ c_2 & D_{21} & D_{22} \end{bmatrix}$$

$$\begin{array}{l} \dot{x} = Ax + Bu \\ y = Cx + Du \end{array}$$

Have  $k: (A-Bk)$  is stable.

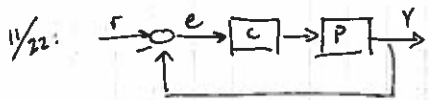
Mapping  $v = ukx; u = v - kx$

$$\dot{x} = (A - Bk)x + Bv; y = (C - Dk)x + Dv; u = v - kx$$

$$P = \frac{Y(s)}{U(s)} = \frac{Y(s)}{V(s)} \cdot \frac{V(s)}{U(s)} = NM^{-1}$$

$$N = \begin{bmatrix} A - Bk & B \\ C - Dk & D \end{bmatrix} \quad M = \begin{bmatrix} A - Bk & B \\ -k & I \end{bmatrix}$$

$u$  to  $y$   $v$  to  $u$



$S = \{H: H \text{ is stable, proper}\}$   
 $P = NM^{-1}$   $N, M \in S$  and coprime  
 Coprime:  $NX + MY = I$ ,  $X, Y \in S$   
 (No shared RHP zeros for  $N, M$ )

Youla parameterization:

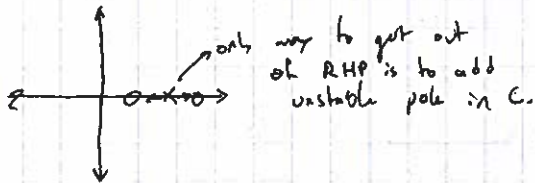
$C$  stabilizing  $\iff C = \frac{X + MQ}{Y - NQ}$ ,  $Q \in S$   
 $S = \frac{1}{1+PC} = M(Y - NQ)$   
 $T = \frac{PC}{1+PC} = N(X + MQ)$

(If  $P$  stable, choose  $N=P, M=1, X=0, Y=1$ )

Strong stabilization:

$P$  is strongly stabilizable if  $\exists C \in S$  that stabilizes the system.

Intuition: Root locus



Theorem:  $P$  is strongly stabilizable  $\iff$  even # of unstable real poles between every pair of "unstable" real zeros (including  $s = +\infty$ )

Proof:  $P = N/M$ ,  $MX + MY = 1$ ,  $M, N, X, Y \in S$   
 $C = (X + MQ)/(Y - NQ)$ ,  $Q \in S$

Suppose  $P$  has zeros at  $\sigma_1, \sigma_2 > 0$ ,  $\sigma_1, \sigma_2 \in \mathbb{R}$

Then  $N(\sigma_1) = N(\sigma_2) = 0$  (because  $M \in S$ )

Suppose have odd # of poles of  $P$  b/w  $\sigma_1/\sigma_2$

Claim that  $M(\sigma_1)$  &  $M(\sigma_2)$  have opposite sign  
 $\rightarrow$  sign of  $M$  as  $s$  go through a zero of  $M$  (pole of  $P$ ) changes from  $+1$  to  $-1$  or vice versa.

$M(\sigma_1)Y(\sigma_1) = 1 = M(\sigma_2)Y(\sigma_2)$

$\Rightarrow Y(\sigma_1)$  &  $Y(\sigma_2)$  have opposite sign.

$C = \frac{X + MQ}{Y - NQ}$   $Y - NQ$  also changes sign between  $\sigma_1$  &  $\sigma_2$

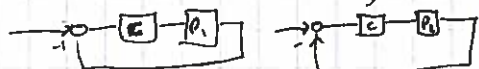
$\Rightarrow Y - NQ$  has at least 1 zero b/w  $\sigma_1$  &  $\sigma_2$

$\Rightarrow C$  has a pole b/w  $\sigma_1$  &  $\sigma_2$  for any  $Q$

Other direction is harder (look in DFT)

Q: when can a single controller  $C$  stabilize two processes  $P_1$  &  $P_2$ ?

(as I am taking off and landing, can I use the same controller for stabilizing both modes?)



$\rightarrow$  Nowadays would just change the rate

Theorem:  $P_1 = N_1/M_1$ ,  $P_2 = N_2/M_2$  are simultaneously stabilizable iff  $P = (N_2 M_1 - N_1 M_2) / (N_2 X_1 + M_2 Y_1) = N/M$  is strongly stabilizable

Proof: Find  $Q_1$  &  $Q_2$  s.t.  $C_1 = \frac{X_1 + M_1 Q_1}{Y_1 - N_1 Q_1} =$

$\frac{X_2 + M_2 Q_2}{Y_2 - N_2 Q_2} = C_2 \iff \exists U \in S$  s.t.

$\begin{cases} X_1 + M_1 Q_1 = U(X_2 + M_2 Q_2) \\ Y_1 - N_1 Q_1 = U(Y_2 - N_2 Q_2) \end{cases}$

algebra  $\rightarrow M + N Q_1 = U \iff M M^{-1} + N N^{-1} C_1 = N C_1 / M C_1$

Q: Given  $(P, C)$  stable, what is the set  $\mathcal{P}$  such that  $(P, C)$  is stable  $\forall P_i \in \mathcal{P}$ .

Chordal Distance:

$d_{RP_2}(w) = \frac{|P_1(jw) - P_2(jw)|}{\sqrt{1 + |P_1(jw)|^2} \sqrt{1 + |P_2(jw)|^2}}$

v-gap metric:  $\delta_v(P_1, P_2) = \begin{cases} \sup_{\omega} d_{P_1, P_2}(w) & \text{if } 1 + P_1(j\omega)P_2(j\omega) \neq 0 \text{ \& \# winding} \\ 1 & \text{o.w.} \end{cases}$  # condition

Generalized stability margin:

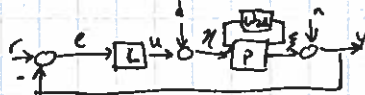
$\sigma_m = \begin{cases} \inf_{\omega} d_{P_1, P_2}(w) & \text{if } C \text{ stabilizes} \\ 0 & \text{o.w.} \end{cases}$

Why  $P_i - \gamma C$ ?

If  $d_{P_i, \gamma C}(w) = 0$   $P_i(w) = \frac{1}{\gamma C(w)} \cdot (1 + P_i(w)C(w)) = 0$

Theorem:  $C$  stabilizes all  $P_i$  s.t.  $\delta_v(P_i, P) < \sigma_m(P, C)$  and "essentially"  $d_{P_1, P_2}(w) < d_{P_i, \gamma C}(w) \forall w$

1/25 Limits on performance: DFT ch. 6



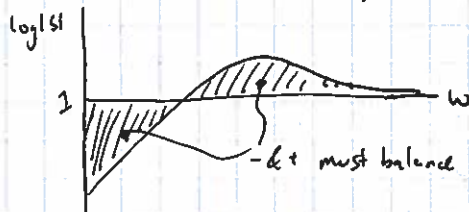
Algebraic limits:

$S + T = 1$ ;  $\|W_p S\| + \|W_r T\|_{\infty} < 1$   
 $\min(|W_p(jw)|, |W_r(jw)|) < 1 \forall w$

\* Bode's Integral Formulation:

Assume rel deg  $L = PC \geq 2$  & internally stable

Theorem:  $\int_0^{\infty} \log |S(jw)| dw = \sum_{\text{poles of } L} \frac{p_i}{p_i + 1}$



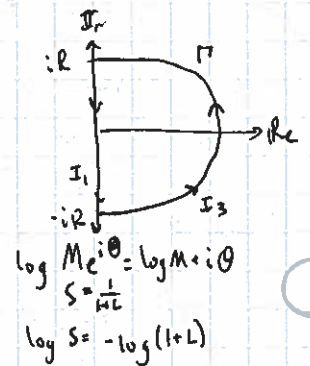
Proof:

$\int_{\Gamma} \log S(s) ds = \lim_{R \rightarrow \infty} I_1 + I_3$

$I_1 = \int_{-R}^R \log |S(jw)| dw$

$= -2i \int_0^R \log |S(jw)| dw$

$I_3 = \int_{-\frac{1}{2}i}^{\frac{1}{2}i} \log(1 + L(R e^{i\theta})) d\theta$   
 $= 0$  if  $L$  has rel deg  $\geq 2$ .





12/4 cont'd: Proof of Lemma 3 in DFT

Lemma 3:  $\forall s_0 = \sigma_0 + j\omega_0$  s.t.  $\sigma_0 > 0$

$$\log |Smp(s_0)| = \frac{1}{\pi} \int_{-\infty}^{\infty} \log |S(j\omega)| \frac{\sigma_0}{\sigma_0^2 + (\omega - \omega_0)^2} d\omega$$

Proof: Use Lemma 1:  $F(s_0) = \frac{1}{\pi} \int_{-\infty}^{\infty} F(j\omega) \frac{\sigma_0}{\sigma_0^2 + (\omega - \omega_0)^2} d\omega$

Plug in  $F(s) = \ln Smp(s)$ , take real part.

$$\text{Re}[F(s)] = \frac{1}{\pi} \int_{-\infty}^{\infty} \text{Re}[F(j\omega)] \frac{\sigma_0}{\sigma_0^2 + (\omega - \omega_0)^2} d\omega$$

$$Smp(s) = e^{F(s)} = e^{\text{Re}[F(s)]} e^{j\text{Im}[F(s)]}$$

$$|Smp(s)| = e^{\text{Re}[F(s)]} \Rightarrow \text{Re}[F(s)] = \ln |Smp(s)| \text{ (LHS)}$$

Since  $S = Smp(s) Sap(s)$  with  $|Sap(s)| = 1$

$$\Rightarrow |S(j\omega)| = |Smp(j\omega)|$$

$$\ln |Smp(s_0)| = \frac{1}{\pi} \int_{-\infty}^{\infty} \ln |S(j\omega)| \frac{\sigma_0}{\sigma_0^2 + (\omega - \omega_0)^2} d\omega.$$

Theorem 1 (Waterbed):

Suppose  $P$  has a zero at  $z$  in RHP. Then  $\exists c_1, c_2$  constants of  $\omega_1, \omega_2, z$  where  $M_1 := \max_{\omega_1 \leq \omega \leq \omega_2} |S(j\omega)|$

$$M_2 := \|S\|_{\infty}$$

$$c_1 \log M_1 + c_2 \log M_2 \geq \log |Sap(z)^{-1}| \geq 0$$

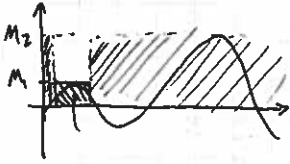
Proof:

$$S(z) = 1 = Smp(z) Sap(z) \Rightarrow Smp(z) = \frac{1}{Sap(z)}$$

$$\log |Smp(z)^{-1}| = \frac{1}{\pi} \int_{-\infty}^{\infty} \log |S(j\omega)| \frac{\sigma_0}{\sigma_0^2 + (\omega - \omega_0)^2} d\omega$$

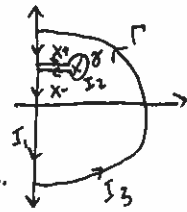
$$c_1 = \frac{1}{\pi} \int_{I_1} \frac{\sigma_0}{\sigma_0^2 + (\omega - \omega_0)^2} d\omega \quad I_1 = [-\omega_2, \omega_1] \cup [\omega_1, \omega_2]$$

$$c_2 = -\int_{I_2} \frac{\sigma_0}{\sigma_0^2 + (\omega - \omega_0)^2} d\omega \quad I_2 = \mathbb{R} \setminus I_1$$



12/25 cont'd:

What if  $L(p_i) = \infty$  for  $p_i \in \text{RHP}$ ?  
 $\int_{\Gamma} \log S(s) ds = \lim_{R \rightarrow \infty} I_1 + I_2 + I_3$



$$I_2 = \int_{\Gamma_1} \log S(s) ds + \int_{\Gamma_2} \log S(s) ds + \int_{\Gamma_3} \log S(s) ds$$

$$= \int_{\Gamma_1} [\log |S(s)| + i \arg S(s)] ds + \int_{\Gamma_2} [\log |S(s)| + i \arg S(s)] ds + \int_{\Gamma_3} [\log |S(s)| + i \arg S(s)] ds$$

cancel          differs by  $2\pi$

$$= 2\pi i \cdot \text{Res}(p_i)$$

Gunter Stein  $\rightarrow$  1<sup>st</sup> Bode Lecture  
 "Respect the unstable"

Theorem: Maximum modulus principle

For any non-constant function  $F: \mathbb{C} \rightarrow \mathbb{C}$  that is analytic on  $\Omega$  closed subset of  $\mathbb{C}$  the maximum of  $|F|$  cannot occur on the interior of  $\Omega$ .

Corollary: Let  $\Omega = \text{RHP}$  (closed) and  $H(s)$  transfer function

w/ no RHP poles:  $\|H\|_{\infty} = \max_{s \in \text{RHP}} |H(s)| \geq |H(s)| \quad \forall s \in \text{RHP}$

Simple Bounds:

$$\|W_p S\|_{\infty} \geq |W_p(z)| \text{ for } z, \text{ a RHP zero of } L(s) = P(s)C(s)$$

$\hookrightarrow$  cannot get good performance around RHP zero.

$$\|W_r T\|_{\infty} \geq |W_r(p)| \text{ for } p, \text{ a RHP pole of } L(s)$$

$\hookrightarrow$  can't get good robustness around RHP poles.

If  $P(s)$  has pole in LHP at  $p_0$ , we can do a pole/zero cancellation

$$P(s) = \frac{n(s)}{d(s)} \quad L(s) = \frac{n(s)}{d(s)} \frac{s+p_0}{s+p_0}$$

"You can cancel all you want in the LHP".

Suppose  $L(s)$  has RHP zero at  $z$  and RHP pole at  $p$ .

$$S = \frac{1}{1+PC} = \frac{dpc}{dpc + nprc} \quad \text{RHP zero at } z.$$

$$S = S_{mp} \cdot \frac{s-p}{s+p} = S_{mp} \cdot S_{ap} \quad S(z) = 1; \quad S_{mp}(z) S_{ap}(z)^{-1} = \frac{z+p}{z-p}$$

$$\|W_p S\|_{\infty} = \|W_p S_{mp}\|_{\infty} \geq |W_p(z) S_{mp}(z)| = |W_p(z) \frac{z+p}{z-p}|$$

RHP pole zero cancellations are not internally stabilizing (unless perfect)...? But they also cause terrible performance.

$$\|W_r T\|_{\infty} \geq |W_r(p) \frac{p+z}{p-z}| \quad p \text{ is RHP pole, } z \text{ is RHP zero of } L(s).$$

★ Ques's question: Suppose you have RHP pole/zero  
 $\hookrightarrow$  Bode integral / Maximum modulus principle  
 What are limits on performance?

Let  $M_1 = \max_{\omega, s, \omega_2} |S(i\omega)|$ ;  $M_2 = \max_{\omega} |S(i\omega)| = \|S\|_{\infty}$

Theorem:  $c_1 \log M_1 + c_2 \log M_2 \geq \log |S_{ap}(z)|^{-1}$  :  $z$  RHP zero of  $L(s)$ .

13/2:

Sample Robust performance criterion:

$$\|W_p S\|_{\infty} + \|W_r T\|_{\infty} < 1$$

weight big when we want  $S$  to be small  
 weight big when model is poor

$T$ : down  $s: r \rightarrow e$  } places where these show up

Limits:

i)  $S+T=1$ .

$$\epsilon \min(|W_p(i\omega)|, |W_r(i\omega)|) < 1 \quad \forall \omega$$

$$ii) \int_0^{\infty} |S(i\omega)| d\omega = \pi \sum_{p_i \in \text{RHP}} \text{Res}(p_i)$$

All-pass transfer functions

$H(s)$  is all-pass if  $|H(i\omega)| = 1 \quad \forall \omega$ .

Ex:  $e^{-\tau s}$ ,  $\frac{s-z}{s+z}$

Theorem: For any  $G(s)$  rational  $\exists G_{mp}, G_{ap}$  rational s.t.  $G = G_{mp} G_{ap}$ ,  $G_{mp}$  is min phase (no RHP poles/zeros) and  $G_{ap}$  is all pass.

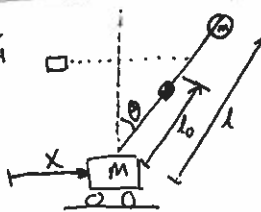
Proof:  $G(s) = \frac{(s+z_1) \dots (s+z_m)}{(s+p_1) \dots (s+p_n)}$   
 suppose  $G(s) = \frac{(s+z_1) \dots (s+z_m)}{(s+p_1) \dots (s+p_n)}$

$$\text{Re}(z_i) > 0; \text{Re}(p_j) > 0$$

$$G_{mp} = \frac{(s+z_1) \dots (s+z_m) (s+z_{r1}) \dots (s+z_r)}{(s+p_1) \dots (s+p_n) (s+p_{r1}) \dots (s+p_r)}$$

$$G_{ap} = \frac{(s-z_{r1}) \dots (s-z_r)}{(s+z_{r1}) \dots (s+z_r)} \cdot \frac{s-z_m}{s+z_m} \cdot \frac{s+p_{n1}}{s-p_{n1}} \dots \frac{s+p_n}{s-p_n}$$

12/4



$$(M+m)\ddot{x} + m l \ddot{\theta} \cos \theta - \dot{\theta}^2 \sin \theta = u + r$$

$$m(\ddot{x} \cos \theta + l \ddot{\theta} - g \sin \theta) = 0$$

$$z = x_0 + l \sin \theta \quad \text{output measurement}$$

$$y = z + n$$

$r =$  activation noise;  $n =$  measurement noise.  
 poles:  $0, \pm \sqrt{\frac{(M+m)g}{M}}$   
 zeros: if  $l_0 < l$ :  $\pm \sqrt{\frac{g}{l-l_0}}$   
 if  $l_0 \geq l$ :  $\pm i \sqrt{\frac{g}{l_0-l}}$   
 $p = z \sqrt{1+r}$   
 $z = \sqrt{\frac{g}{z}}$   
 $r = \frac{m}{M}$

Interpretation:  $\lambda \lambda$

$$\|W_r T\|_{\infty} \geq |W_r(p) \frac{p+z}{p-z}|$$

12/6: Review: "If you didn't have a HW, it won't be there"

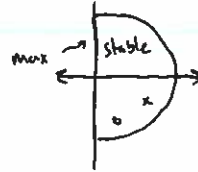
• Youla parameterization. Not as much algebra.

THE LIST:

- ?? • Maximum Principle
- X • Coprime factorization
- ✓ • Robust Performance
- ✓ • LQR
- ? • Linear observers
- ?? • Kalman decomposition
- ✓ • A invariant subspaces
- ?? • Youla parameterization
- X • Robust stability/performance with two uncertainties
- X • Induced norms
- ✓ • Observability tests
- ✓ • Stability tests
- X • Bode's integral formula
- X • MIMO small gain
- X • Chordal/v-gap
- ✓ • Limits of performance
- ✓ • Controllability/observability Gramians
- X • Phase margin
- X • Bode plots
- ??? • Nyquist plots
- ✓ • Solution of linear input/output systems
- ? • Convolution
- ✓ • Block diagram [there's one in the exam]
- ? ↳ not a lot of block diagram algebra

Limits of Performance:

- Check first for stability
- Algebraic limits → always true
- Integral formulas [e.g. water bed effect]
  - ↳ mostly won't ask about integral formulas
- Maximum modulus principle → know and be able to apply
  - ↳ if stable & bounded, max will occur on jw axis.



$$S(z)=1 \quad S(p)=0 \quad S=\frac{1}{1+PC}$$

$$T(z)=0 \quad T(p)=1 \quad T=\frac{PC}{1+PC}$$

$$\|WpS\|_{\infty} \geq Wp(s)S(s) \quad \forall s \in \text{RHP}$$

$$\|Hap\|_{\infty} = 1$$

$$\|H \cdot Hap\|_{\infty} = \|H\|_{\infty}$$

→ how to do all phase } manipulate problem

$$S = \frac{1}{1+PC} = \frac{z-p}{z+p} = Smp \cdot \frac{z-p}{z+p}$$

$$S=1 = Smp Sap$$

$$Smp = Sap^{-1}$$

$$\|WpS\|_{\infty} = \|WpSmp\|_{\infty} \geq Wp \frac{z-p}{z+p}$$

RHP pole zero ⇒ using Sap & factorization

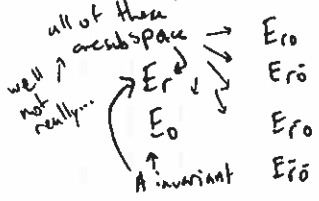
A-invariant Subspaces:

Definition:  $V \subset \mathbb{R}^n \quad AV \subset V \quad v \in V$

Fact: reachable space is the smallest A-invariant space containing B

Fact: unobservable space is the largest A-invariant space annihilated by C  
 ↳ start with B. if it's invariant then AB must be in there  
 ... Look at  $A^2B$ , etc when this stops growing, it's the largest

A invariant space containing B.



$E_0 \rightarrow$  only A-invariant space

$E_0$  is not a subspace it is the complement to  $E_0$

LQR:

$$L = \int_0^T (x^T Q x + u^T R u) dt \quad Q \geq 0, R \geq 0$$

$$\dot{P} = PA + AP + PB(R^{-1}B^T)P, P(T) = P_0$$

↳ fell out from maximum principle

↳ Riccati equation:

$$u = -R^{-1}B^T P x$$

→ stabilizing properties of LQR

→ consequences of if Q & R are not > 0

★ Where do the equations come from, what do they mean, etc...?

Robust Performance: → where do these come from?

Robust performance ⇔ robust stability + performance →  $\|WpS\|_{\infty} \leq 1$

↑ knowing this

↑ can I manipulate this into some form?

→ ex:  $\|WpS\| + \|W_r T\|_{\infty} < 1$

Necessary: if this is satisfied, then I can find a controller  
 ↳ show how you would find this.

*[Faint, illegible text, likely bleed-through from the reverse side of the page]*

